Multiscale Simulation of Porous Media Flow: Obstacles, Opportunities and Open-source SIAG/GS Early Career Prize Lecture

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Porous media flow – a multiscale problem



Layered geological structures typically occur on both large and small scales

Porous media flow – a multiscale problem

The scales that impact fluid flow in subsurface rocks range from

- the micrometer scale of pores and pore channels
- via dm-m scale of well bores and laminae sediments
- to sedimentary structures that stretch across entire reservoirs

Porous rocks are heterogeneous at all length scales (no scale separation)



Numerical methods that attempt to model physical phenomena on coarse grids while honoring small-scale features in an appropriate way consistent with the local property of the differential operator



From Poisson's equation to reservoir simulation



Multiscale finite-volume methods – status in 2013

Extensive research over the past 15 years – more than 60 papers by Jenny, Lee, Tchelepi, Lunati, Hajibeygi, and others:

- correction functions to handle non-elliptic features
- extension to compressible flow
- adaptivity in updating of basis functions
- iterative formulation with smoothers (Jacobi, GMRES, ...)
- algebraic formulation

.

fracture models (embedded/hierarchical, etc)

Strong focus on the ability to converge to a fine-scale solution has gradually made MsFV similar to multigrid methods

Fine-scale system $-\nabla \cdot \mathbf{K} \nabla p = q$ Ax = b



Fine-scale system $-\nabla \cdot \mathbf{K} \nabla p = q$ Х Ax = bUpscaling $-\nabla \cdot \mathbf{K}_c \nabla p_c = q_c$ X_c $\mathbf{x}_c =$ b_c $A_c x_c = b_c$



Fine-scale system $-\nabla \cdot \mathbf{K} \nabla p = q$ Х Ax = bUpscaling $-\nabla \cdot \mathbf{K}_c \nabla p_c = q_c$ X_c b_c $A_c x_c = b_c$ Multiscale method P = basis(A) Px_m $\mathbf{x}_m =$ b_m $x \approx P x_m$ Restriction: R

Qualitatively correct \rightarrow small residual



Qualitatively correct \rightarrow small residual



Qualitatively correct \rightarrow small residual

Residual iteration:

computational cost





Hou & Wu (1996) Jenny, Lee, Tchelepi (2003)







The multiscale finite-volume (MsFV) method



- Localization assumption: lower-dimensional local solution as approximation
- Generally: successive approximation 1D \rightarrow 2D \rightarrow 3D

The missing piece: industry-standard simulation models

- MsFV only applied to Cartesian grids and idealized versions of real flow physics
- Localization \rightarrow unstable multipoint coarse-scale stencil gives oscillatory solutions
- Requirement of consistent dual-primal partition makes coarsening difficult
- For industry use: needs automated and robust coarsening



SPE 10: $\log(K)$



Reference solution



MsFV solution

























Why is this challenging?



Grid models represent the reservoir geology and are known to have many obscure features $% \left({{{\mathbf{r}}_{\mathrm{s}}}} \right)$

Challenges:

- Industry standard: corner-point / stratigraphic grids
- Grid topology is unstructured because of faults, pinch-outs, erosion, inactive cells, etc
- Geometry: deviates from box shape, high aspect ratios, many faces/neighbors, small faces, ...
- Petrophysics: orders of magnitude variations between neighboring cells
 Coarse grids:
 - Will be unstructured as a general rule
 - Will have strange shapes, many special cases to be handled
 - Should adapt to features in the reservoir model: petrophysical properties, faults, flow units, flow directions, wells, ...

First contribution: MsFV for unstructured grids



Algorithm for generating admissible primal-dual partitions on general grids

- geometrical partitioning using triangulation
- automated on rectilinear, curvilinear, triangular, and Voronoi grids
- semi-automated on corner-point grids and grids with non-matching faces
- monotonicity issues for heterogeneous permeability

Møyner & Lie: The multiscale finite-volume method on stratigraphic grids, SPE J. (2013)

Localization assumption – difficult to impose



Challenge: How to solve representative local problem from A to B?

Difficulties – thick edges



- Edge cells must be connected through faces to solve reduced flow problem between block centers → thick and interwoven edges, ill suited for numerics
- Difficult to do either graph or geometric algorithms

Difficult to automate partitioning for complex grids

Rethinking the prolongation operator: First attempt



- Simultaneously worked on flow-diagnostics for rapid evaluation of models
- Combine partition-of-unity tracer solutions with local upscaling for basis
- Trades some accuracy for robustness and works on general grids
- In the end, too complicated! Back to the drawing board...

Møyner & Lie: A multiscale two-point flux-approximation method, J. Comput. Phys (2014) Møyner, Krogstad & Lie: The application of flow diagnostics for reservoir management, SPE J. (2014)

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Rethinking the prolongation operator: Another attempt

What are our requirements on the prolongation operator P?

- Partition of unity: represent constant fields $\sum_{j=1}^{N} P_{ij} = 1 \longrightarrow \text{Exact interpolation of constant modes}$
- Algebraically smooth: minimize $||AP||_1$ implies that $APp_c \approx Ap$ locally
- Localization: coarse system $A_c = RAP$ becomes denser as the support of basis functions grows

Approach inspired by smoothed aggregation multigrid (Vaněk et al, 1996)

MsRSB: multiscale restriction-smoothed basis



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Set P_j to one inside block j





Jacobi increment:
$$d_j = -\omega D^{-1} A P_j^n$$







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Localize update:

$$\hat{d}_{ij} = \begin{cases} d_i \\ \end{pmatrix}$$





Indices: $i = \text{cell}, j = \bigcirc, k = \bigcirc$



Jacobi increment:
$$d_j = -\omega D^{-1} A P_j^n$$

Localize update:

$$\hat{d}_{ij} = \begin{cases} d_{ij} \\ 0 \end{cases}$$





Indices: $i = \text{cell}, j = \bigcirc, k = \bigcirc$



Support region: computed upfront by triangulating coarse centroids

Jacobi increment:
$$d_j = -\omega D^{-1} A P_j^n$$

Localize update:

$$\hat{d}_{ij} = egin{cases} \displaystyle rac{d_{ij}}{0} \ \displaystyle rac{d_{ij} - P_{ij}^n \sum_k d_{ik}}{1 + \sum_k d_{ik}} \end{cases}$$

Indices:
$$i = \text{cell}, j = \bigcirc, k = \bigcirc$$

Apply increment:
$$P_{ij}^{n+1} = P_{ij}^n + \hat{d}_{ij}$$






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Apply increment: $P_{ij}^{n+1} = P_{ij}^n + \hat{d}_{ij}$

Repeat until convergence







MsRSB: Support regions

Basis functions require a coarse grid and a support region

- Support region: logical indices, topological search, distance measures,...
- Region constructed using triangulation of nodal coarse neighbors, resulting in an MPFA stencil on the coarse scale
- Main point: Easy to implement in 3D for fully unstructured meshes



Coarse grid and local triangulation



Interaction region and boundary



Resulting basis function

MsRSB: Support regions

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Coarse grid and local triangulation





SPE10 – Full model 2



Horizontal permeability



MsRSB



Reference solution



MsFV,

Error	Grid	p (L ₂)	p (L_{∞})	v (L ₂)	v (L_{∞})
MsFV	$6\times11\times17$	3.580	128.461	2.288	11.957
MsRSB	$6\times11\times17$	0.039	0.309	0.397	0.487

SPE10 – Full model 2



Horizontal permeability



MsRSB



Reference solution



MsFV, $p \not\in [0,1]$

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Example: unstructured PEBI grid



Porosity and grid



Permability from SPE 10, Layer 35





Detailed view of refinement

- Unstructured grid designed to minimize grid orientation effects
- Two embedded radial grids near wells
- Fine grid adapts to faults
- The faults are sealed, i.e. allow no fluid flow through

Example: unstructured PEBI grid



Two-step preconditioner, ILU(0) as 2nd stage, Richardson iterations

Example: unstructured PEBI grid



Two-step preconditioner, ILU(0) as 2nd stage, Richardson iterations

Two-phase flow, PEBI grid



Fine-scale (around 6000 dof)

Multiscale (146 dof)

Two-phase flow, PEBI grid



Fine-scale (around 6000 dof)

Multiscale (146 dof)

Two-phase flow, PEBI grid



Fine-scale (around 6000 dof)

Multiscale (146 dof)

Introduction: The Gullfaks field



- Field from the North Sea in Norway challenging anisotropic permeability and grid
- Model includes cells with nearly 40 faces
- 216 000 cells with a large number of faults and eroded layers
- Synthetic well configuration with four vertical wells

The Gullfaks field – incompressible flow

- First coarsening strategy: Uniform blocks, split over faults
- Second coarsening strategy: Use Metis with same number of DoF

Grid type	DoF	р (<i>L</i> ₂)	p (L_{∞})
$15\times15\times20$	416	0.032	0.102
Metis	416	0.032	0.100
$10\times10\times10$	1028	0.028	0.597
Metis	1028	0.015	0.112



The Gullfaks field – incompressible flow



MsRSB (416 DoF)

Extensions of MsRSB



Møyner & Lie, SPE J. (2017)

Black-oil & compressible multiphase flow

Polymer EOR with non-linear velocity



Hilden et al, TiPM. (2017)

Embedded fracture models



Shah et al, JCP (2016)



- - P2 M

Multiple feature-specific operators



Lie et al, SPE J (2016) Klemetsdal et al, COMG (2019)

Gullfaks field - simulated in Intersect Multiscale simulator



- Giant North Sea field, started production in 1986
- Sedimentology similar to SPE 10, but heavily faulted
- Mainly water injection, but also gas and water-alternating-gas in some areas
- \blacksquare Coarse $80 \times 100 \times 19$ black-oil simulation model with real history

Lie, Møyner, Natvig, Kozlova, Bratvedt, and Watanabe - Successful Application of Multiscale Methods in a Real Reservoir Simulator Environment Comput. Geosci. (2017)

Gullfaks field - simulated in Intersect Multiscale simulator



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 f_i^L

• EoS-coupled compositional flow with N components $i \in \{1, ..., N\}$,

$$\frac{\partial}{\partial t} (\phi \left[\rho_L S_L X_i + \rho_V S_V Y_i\right]) + \nabla \cdot (\rho_L X_i \vec{v}_L + \rho_V Y_i \vec{v}_V) = q_i,$$
$$\vec{v}_\alpha = -\mathbf{K} \lambda_\alpha (\nabla p_\alpha - \rho_\alpha g \Delta z)$$
$$(p, T, x_1, ..., x_N) = f_i^V (p, T, y_1, ..., y_N) \sum_{i=1}^N x_i = 1, \sum_{i=1}^N y_i = 1, S_V + S_L = 1.$$

- Multiscale solver is most efficient in a sequential setting
- Objective: Sequential-implicit scheme for EoS-compositional flow
- Many schemes in literature often simplified compositional descriptions or insufficient details given



First attempt: Total mass-based scheme (Møyner & Tchelepi, RSC17)



• First attempt: Total mass-based scheme (Møyner & Tchelepi, RSC17) \rightarrow failure.

Stability of previously suggested scheme fails for general fluid description

- Again, it was back to the drawing board: Literature study, discussions with Arthur Moncorgé at Total, a few failed prototypes...
- Transport with relaxed saturation closure, volumetric pressure equation
- Exact mass-conservation without outer loop
- Compatible with natural or molar variables



Møyner & Tchelepi - A Mass-Conservative Sequential Implicit Multiscale Method for General Compositional Problems, SPE J. (2018) Historical works: Acs et al (1985), Watts (1986), Trangenstein & Bell (1989), Coats (1995), ...

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Compositional Norne: Gas production



Compositional Norne: Gas production



Multiscale Norne - Linear solver time



There are substantial research challenges and opportunities in applying methods to industrial test cases

- Test your methods on as real problems as possible, as early as possible
- Fail fast fail often. Solutions never arrive as fully-formed ideas
- Kill your darlings don't get attached to the first almost working solution

How to do this efficiently? Develop open-source code.

- Build on the work of others, and let others build on your work
- Reproducible science: Version control, systematic storage of test cases
- Releasing code means cleaning up, documenting and making it ready for the next project!

The MATLAB Reservoir Simulation Toolbox

Open-source toolbox for reservoir modelling, developed by SINTEF Digital and used in most of our research

Wide international user base:

- academic institutions, oil and service companies
- USA, Norway, China, Brazil, United Kingdom, Iran, Germany, Netherlands, France, Canada, ...
- 9000+ unique downloads last two years

MRST - MATLAB Reservoir Simu	lation Toolbox		SEARCH
MRST FAG Follow Module			
The Matlab Reservoir Simul	ation Toolbox		
Beele functionality	Discretizations and solvers	Workfow tools	
Department of Applied Mathematics at SP	VTCP /CT, F Becamber 2016, and can be downloaded under the letter of	Download	

http://www.sintef.no/
http://www.bitbucket.org/mrst/

Used in publications:

- 130+ master and PhD theses
- 210+ journal/proceedings papers by authors outside our group

General object-oriented framework for porous media flow

- Extended MRST from discretization framework to general multiphysics capabilities
- Modular code easy to swap components
- Multiphase flow, thermal, tracers, geomechanics, compositional, black-oil, geochemistry, multisegment wells ...



MRST AD-OO – surprisingly efficient

What can you do with MRST-OO? Assembly of three-phase problem with two wells





Collaborators at SINTEF, NTNU, Stanford, TU Delft, Chevron and Schlumberger

Funding

- Research Council of Norway as a part of grant 226035
- VISTA, a basic research programme funded by Equinor and conducted in close collaboration with The Norwegian Academy of Science and Letters

We are hiring - tinyurl.com/sintef-comg-2019

Backup

Compositional model in the Matlab Reservoir Simulation Toolbox (MRST) has typical choices for compositional simulation of hydrocarbons,

- Densities and phase behavior predicted by equation-of-state
- Generalized cubic equation-of-state: Martin's equation
- Lohrenz-Bray-Clark viscosity correlations
- Schur-complement used to obtain N by N system for variable set α ,

$$-J\Delta x = \begin{bmatrix} B & C \\ D & E \end{bmatrix} \begin{bmatrix} \alpha \\ \beta \end{bmatrix} = \begin{bmatrix} f \\ h \end{bmatrix} \to A\alpha = (B - CE^{-1}D)\alpha = f - CE^{-1}h = b.$$

Remark: E is easily invertible, as fugacity is local to each cell

Pressure

Assemble backward Euler accumulation terms and fugacities,

$$C_{i} = \frac{\Phi}{\Delta t} \left[(\rho_{L}S_{L}X_{i} + \rho_{V}S_{V}Y_{i})^{n+1} - (\rho_{L}S_{L}X_{i} + \rho_{V}S_{V}Y_{i})^{0} \right]$$

$$F_{i} = f_{i}^{L}(p, T, x_{1}, ..., x_{N}) - f_{i}^{V}(p, T, y_{1}, ..., y_{N}).$$

Reduce this system R to $N \times N$ primary variables p by eliminating secondary variables s,

$$R = \begin{bmatrix} \frac{\partial C}{\partial p} & \frac{\partial C}{\partial s} \\ \frac{\partial F}{\partial p} & \frac{\partial F}{\partial s} \end{bmatrix} \to G = \left(\frac{\partial C}{\partial p} - \frac{\partial C}{\partial s} \frac{\partial F}{\partial s}^{-1} \frac{\partial F}{\partial p} \right)$$

Find weights that eliminate time-derivatives for non-pressure variables

$$(G^T)^{-1}w = e_i \begin{cases} 1 \text{ if variable i is pressure} \\ 0 \text{ otherwise} \end{cases}$$

Pressure equation is linear combination of component mass conservation,

$$R_p = \sum_{i=1}^{N} w_i M_i$$
, which removes any volume error from transport.

Sequential scheme: Transport

• Again, conservation of each component $i \in \{1, ..., N\}$ with fixed pressure,

$$\frac{\partial}{\partial t} (\phi \left[\rho_L S_L X_i + \rho_V S_V Y_i \right]) + \nabla \cdot (\rho_L X_i \vec{v}_L + \rho_V Y_i \vec{v}_V) = q_i,$$

with fugacity balance in two-phase cells.

Sum of mole fractions close the system, but saturation closure is relaxed

$$\sum_{i=1}^{N} x_i = 1, \sum_{i=1}^{N} y_i = 1, \quad S_V \ge 0, \ S_L \ge 0.$$

• Removal of one variable and one equation \rightarrow system is still well-posed Component fluxes are given by fractional flow, accounting for volume error:

$$\vec{v}_{i,L} = \tilde{X}_i F_L (\vec{v}_T + \sum_{\beta \neq L} \lambda_\beta \mathbf{K} (\rho_L - \rho_\beta)),$$

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$$(42/36)$$