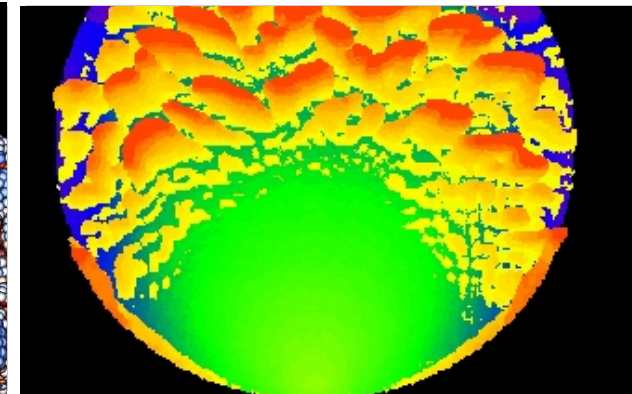
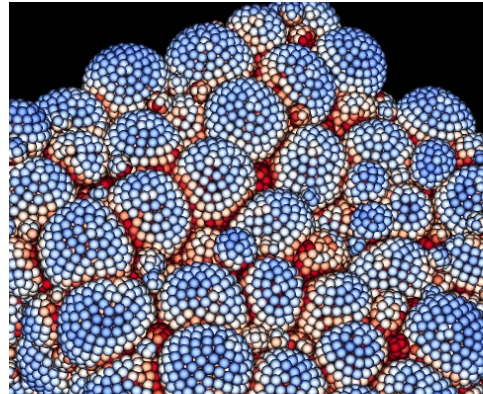
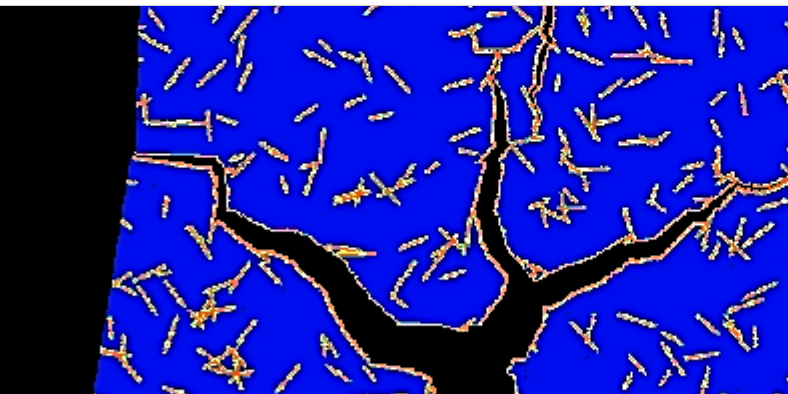


Exceptional service in the national interest



Modeling microstructure and defects with peridynamics

Stewart Silling

Sandia National Laboratories

Albuquerque, New Mexico

SIAM Conference on Mathematical Aspects of Materials Science, Portland, OR, July 11, 2018

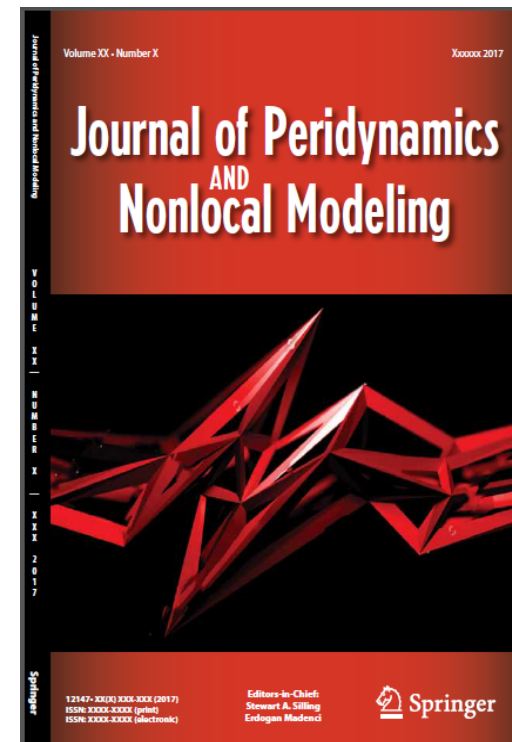


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Outline

- Peridynamic theory summary
- Defects and material failure
- Phase changes and microstructure

New journal from Springer Nature
First issue Jan 2019



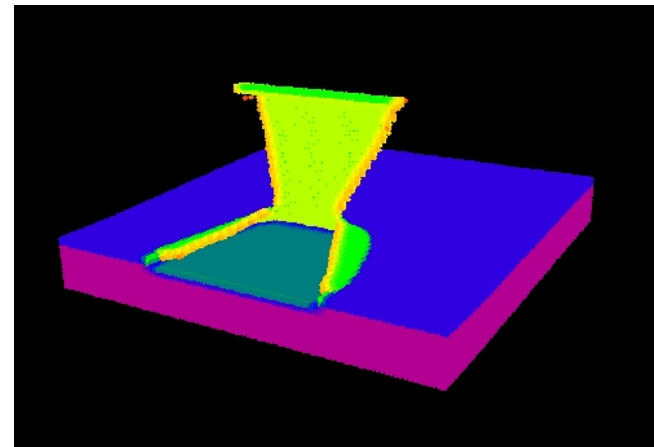
Gaps in classical continuum mechanics

- Momentum balance, 1D:

$$\rho u_{tt} = (\sigma(u_x))_x + b$$

where u =displacement, σ =stress, b =external body force.

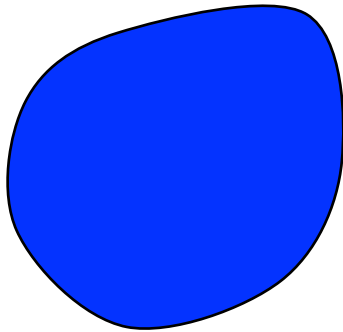
- Requires u to be twice continuously differentiable.
- Doesn't apply on cracks or growing discontinuities.
- Predicts infinite stress near defects.
- Can't include nanoscale forces.



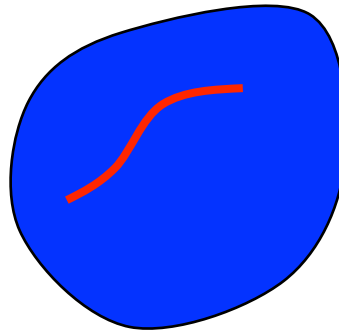
Humble Scotch[®] tape

Peridynamics:* What it is

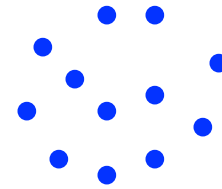
- It's an extension of continuum mechanics to media with cracks and long-range forces.
- It unifies the mechanics of continuous and discontinuous media within a single, consistent set of equations.



Continuous body



Continuous body
with a defect



Discrete particles

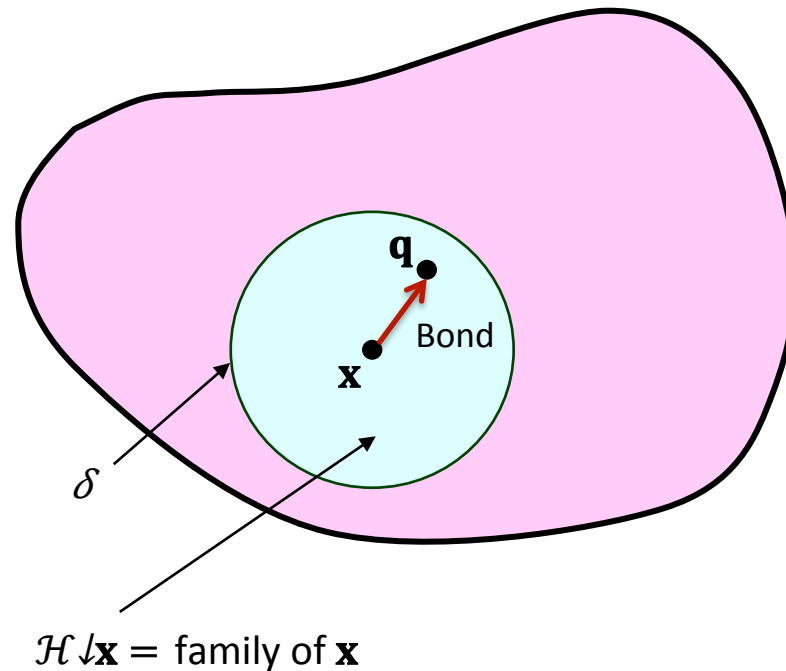
- Our goals
 - Nucleate cracks and seamlessly transition to growth.
 - Model complex fracture patterns.
 - Communicate across length scales.

* Peri (near) + dyn (force)

Peridynamics concepts:

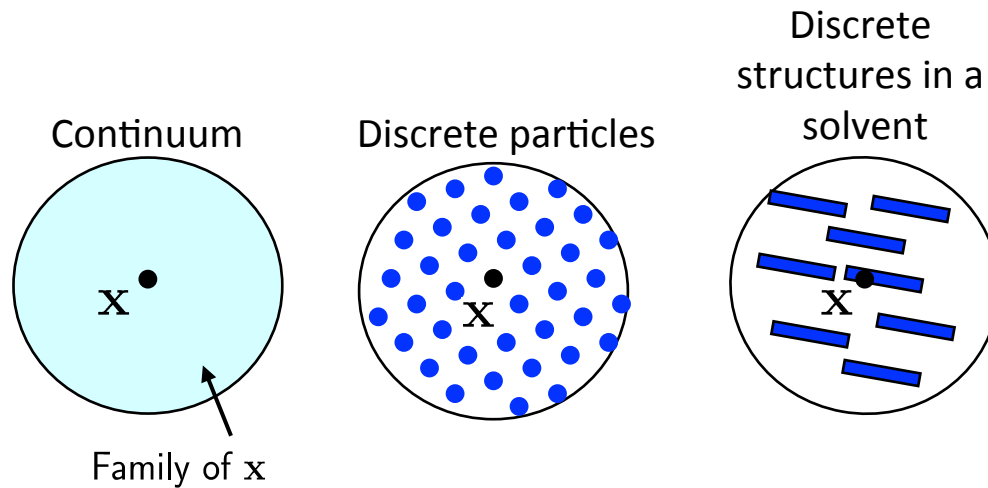
Horizon and family

- Any point \mathbf{x} interacts directly with other points within a distance δ called the “horizon.”
- The material within a distance δ of \mathbf{x} is called the “family” of \mathbf{x} , $\mathcal{H}_{\mathbf{x}}$.

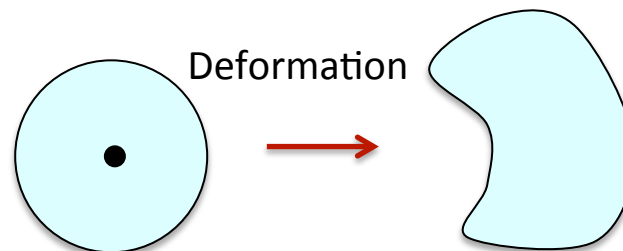


- SS, *J. Mechanics and Physics of Solids* (2000)
- SS & Lehoucq, *Advances in Applied Mechanics* (2010)

Peridynamic concept of strain energy density at a point

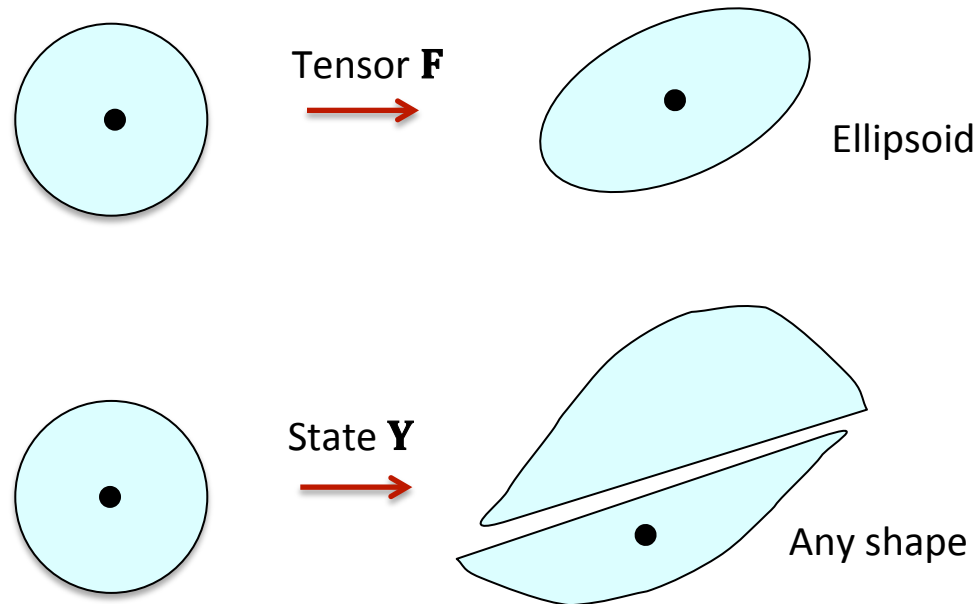


- The strain energy density $W(\mathbf{x})$ is determined by the deformation of the entire family of \mathbf{x} .
- How to describe this dependence? **States**



States: Nonlinear analogues of second order tensors

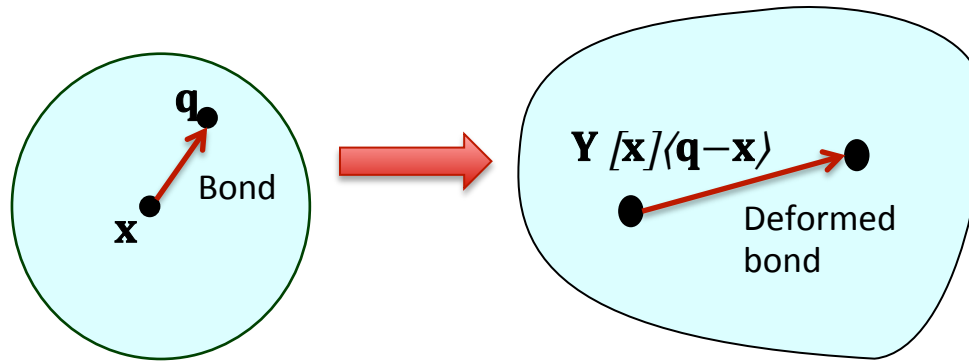
- Classical theory uses tensors (linear mappings from vectors to vectors).
- Peridynamics uses states (nonlinear mappings from vectors to vectors).



States

- A *state* is a mapping whose domain is all the bonds ξ in a family.

$$\underline{\mathbf{A}}\langle\xi\rangle = \text{something} \quad \forall \xi \in \mathcal{H}.$$



- Deformation state...

$$\underline{\mathbf{Y}}[\mathbf{x}]\langle\mathbf{q}-\mathbf{x}\rangle = \mathbf{y}(\mathbf{q}) - \mathbf{y}(\mathbf{x}) = \text{deformed image of the bond}$$

Strain energy density: $W(\mathbf{Y})$

Operations with states

- Two operators on states are defined by

$$\underline{\mathbf{A}} \bullet \underline{\mathbf{B}} = \int_{\mathcal{H}} \underline{\mathbf{A}}\langle \xi \rangle \cdot \underline{\mathbf{B}}\langle \xi \rangle dV_{\xi} \quad \dots \text{dot product (a scalar)}$$

$$\underline{\mathbf{A}} \star \underline{\mathbf{B}} = \int_{\mathcal{H}} \underline{\mathbf{A}}\langle \xi \rangle \otimes \underline{\mathbf{B}}\langle \xi \rangle dV_{\xi} \quad \dots \text{tensor product (a 2nd order tensor)}$$

- Two more useful states...

$$\underline{\mathbf{1}}\langle \xi \rangle = 1 \quad \forall \xi \in \mathcal{H} \quad \dots \text{unity state,}$$

$$\underline{\mathbf{X}}\langle \xi \rangle = \xi \quad \forall \xi \in \mathcal{H} \quad \dots \text{identity state.}$$

Functions of states

- Let $\Psi(\underline{\mathbf{A}})$ be a scalar-valued function of a state.
- Suppose there is a state $\Psi_{\underline{\mathbf{A}}}(\underline{\mathbf{A}})$ such that for any small increment $d\underline{\mathbf{A}}$,

$$\Psi(\underline{\mathbf{A}} + d\underline{\mathbf{A}}) - \Psi(\underline{\mathbf{A}}) = \Psi_{\underline{\mathbf{A}}}(\underline{\mathbf{A}}) \bullet d\underline{\mathbf{A}}.$$

- Then $\Psi_{\underline{\mathbf{A}}}(\underline{\mathbf{A}})$ is the *Fréchet derivative* of Ψ at $\underline{\mathbf{A}}$.

Potential energy minimization yields the peridynamic equilibrium equation

- Potential energy:

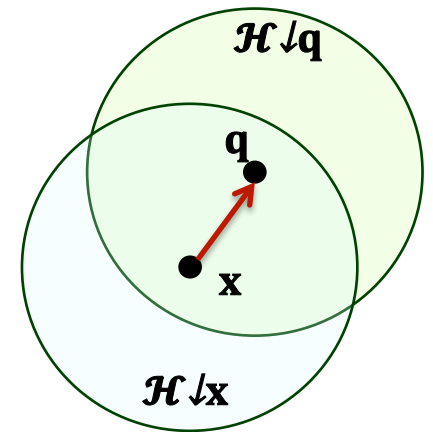
$$\Phi = \int_{\mathcal{B}} (W - \mathbf{b} \cdot \mathbf{y}) dV_{\mathbf{x}}$$

where W is the strain energy density, \mathbf{y} is the deformation map, \mathbf{b} is the applied external force density, and \mathcal{B} is the body.

- Euler-Lagrange equation is the equilibrium equation:

$$\int_{\mathcal{H}_{\mathbf{x}}} \mathbf{f}(\mathbf{q}, \mathbf{x}) dV_{\mathbf{q}} + \mathbf{b}(\mathbf{x}) = 0$$

for all \mathbf{x} . \mathbf{f} is the *pairwise bond force density*.



- \mathbf{f} is found from the Fréchet derivatives of W at \mathbf{x} and each \mathbf{q} :

$$\mathbf{f}(\mathbf{q}, \mathbf{x}) = W_{\underline{\mathbf{Y}}}[\mathbf{x}] \langle \mathbf{q} - \mathbf{x} \rangle - W_{\underline{\mathbf{Y}}}[\mathbf{q}] \langle \mathbf{x} - \mathbf{q} \rangle.$$

Material models

- Recall the equilibrium equation:

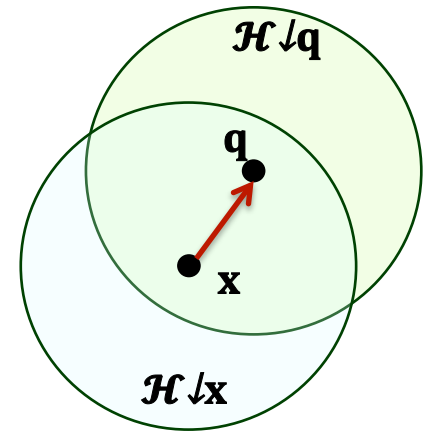
$$\int_{\mathcal{H}} \mathbf{f}(\mathbf{q}, \mathbf{x}) + \mathbf{b}(\mathbf{x}) = \mathbf{0}$$

where (from the first variation of Φ)

$$\mathbf{f}(\mathbf{q}, \mathbf{x}) = \underline{\mathbf{T}}[\mathbf{x}] \langle \mathbf{q} - \mathbf{x} \rangle - \underline{\mathbf{T}}[\mathbf{q}] \langle \mathbf{x} - \mathbf{q} \rangle.$$

- $\underline{\mathbf{T}}[\mathbf{x}]$ is the *force state* obtained from the material model $\hat{\underline{\mathbf{T}}}$ applied to the family of \mathbf{x} :

$$\underline{\mathbf{T}}[\mathbf{x}] = \hat{\underline{\mathbf{T}}}(\underline{\mathbf{Y}}[\mathbf{x}]).$$



- SS, Epton, Weckner, Xu, & Askari, *J. Elasticity* (2007)

Examples of material models

- Bond-based (each bond responds independently of the others):

$$\underline{\mathbf{T}}\langle\xi\rangle = f(s, \xi) \frac{\underline{\mathbf{Y}}\langle\xi\rangle}{|\underline{\mathbf{Y}}\langle\xi\rangle|}, \quad s = \frac{|\underline{\mathbf{Y}}\langle\xi\rangle| - |\xi|}{|\xi|}$$

where s =bond strain.

Direction of the deformed bond ξ

- Isotropic solid:

$$\underline{\mathbf{T}}\langle\xi\rangle = \alpha s + \beta \vartheta, \quad \vartheta = \underline{\mathbf{U}} \bullet \underline{\mathbf{X}}, \quad \underline{\mathbf{U}} = \underline{\mathbf{Y}} - \underline{\mathbf{X}}$$

where α, β are constants and ϑ is a measure of the volume change in the family, and $\underline{\mathbf{U}}$ =displacement state.

- Linearized:

$$\underline{\mathbf{T}} = \underline{\mathbf{K}} \bullet \underline{\mathbf{U}}, \quad \underline{\mathbf{K}} = W_{\underline{\mathbf{Y}}\underline{\mathbf{Y}}}$$

where $\underline{\mathbf{K}}$ is the micromodulus double state (second Fréchet derivative).

$$\underline{\mathbf{T}}\langle\xi\rangle = \int_{\mathcal{H}} \underline{\mathbf{K}}\langle\xi, \zeta\rangle \cdot \underline{\mathbf{U}}\langle\zeta\rangle dV_{\zeta}.$$

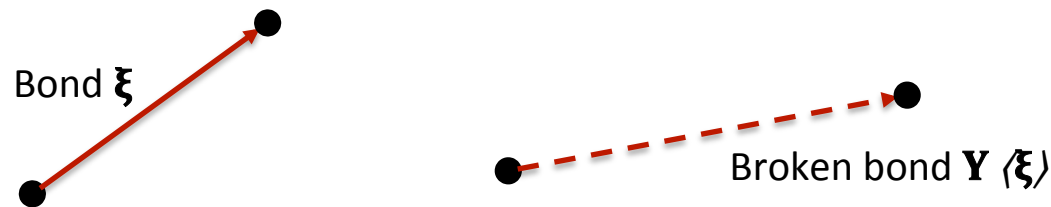
Damage

- Damage is usually treated through *bond breakage*.
- After a bond ξ *breaks* according to some criterion, it no longer carries any force.
- Typical breakage criterion: prescribed *critical bond strain* s_0 :

$$s = \frac{|\underline{\mathbf{Y}}\langle\xi\rangle| - |\xi|}{|\xi|} \quad \text{bond strain.}$$

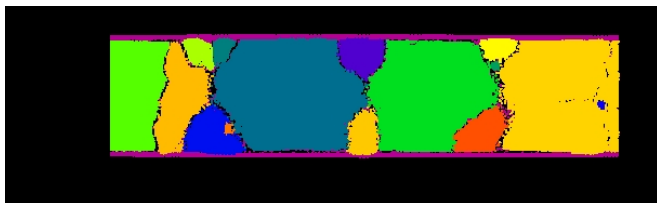
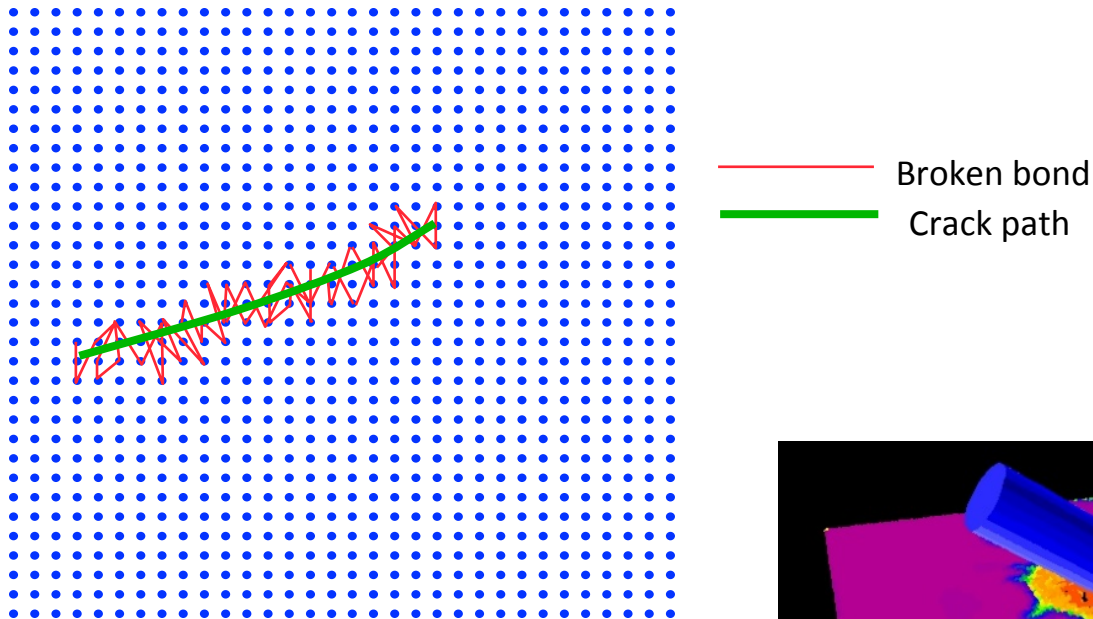
$$s \geq s_0 \text{ at some time } t_0$$

means the bond remains broken for all $t \geq t_0$.

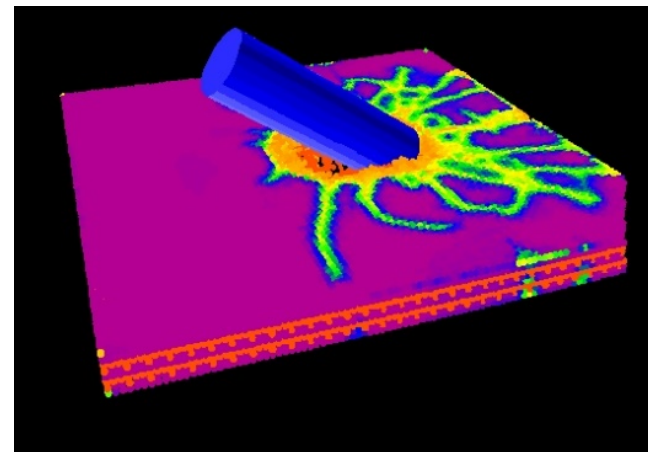


Discontinuities are treated within the basic field equations

- When a bond breaks, its load is shifted to its neighbors, leading to progressive failure.



Cracking in a composite lamina

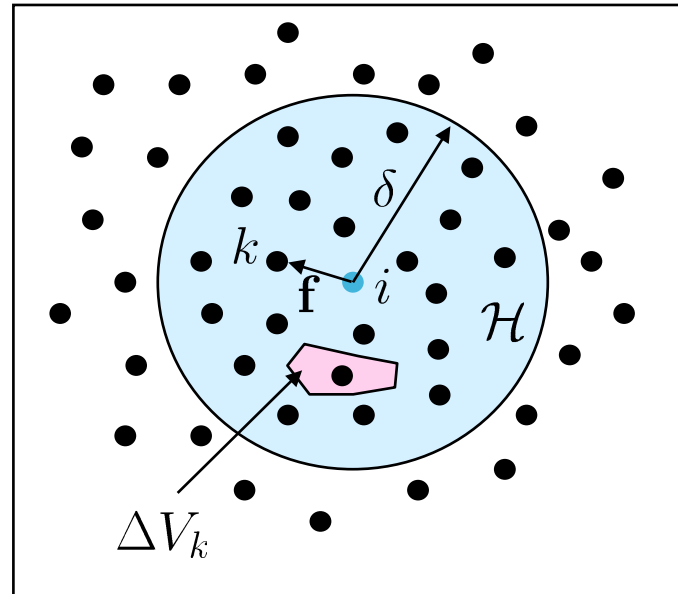


Impact against reinforced concrete

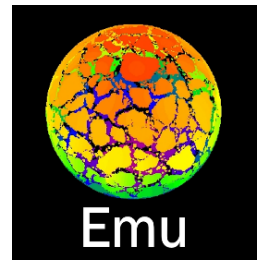
Emu numerical method

- Integral is replaced by a finite sum: resulting method is [meshless](#) and [Lagrangian](#).

$$\rho \ddot{\mathbf{y}}(\mathbf{x}, t) = \int_{\mathcal{H}} \mathbf{f}(\mathbf{x}', \mathbf{x}, t) dV_{\mathbf{x}'} + \mathbf{b}(\mathbf{x}, t) \quad \longrightarrow \quad \rho \ddot{\mathbf{y}}_i^n = \sum_{k \in \mathcal{H}} \mathbf{f}(\mathbf{x}_k, \mathbf{x}_i, t) \Delta V_k + \mathbf{b}_i^n$$



- SS & Askari, *Computers & Structures* (2005)
- Tian & Du, *SIAM Journal on Numerical Analysis* (2014)



Force states and stress

- For a homogeneous deformation of a homogeneous body,

$$\boldsymbol{\sigma} = \underline{\mathbf{T}} \star \underline{\mathbf{X}} \quad \text{or} \quad \boldsymbol{\sigma} = \int_{\mathcal{H}} \underline{\mathbf{T}}\langle \boldsymbol{\xi} \rangle \otimes \boldsymbol{\xi} \, dV_{\boldsymbol{\xi}}.$$

- This $\boldsymbol{\sigma}$ is called the *partial stress*.
- It has the usual mechanical interpretation (force/area).
- For non-homogeneous deformations, in general for this $\boldsymbol{\sigma}$

$$\nabla \cdot \boldsymbol{\sigma} + \mathbf{b} \neq \mathbf{0}.$$

- But there is a more general peridynamic stress tensor for which equality holds.

- Lehoucq & SS, *J. Mechanics and Physics of Solids* (2008)
- SS, Littlewood & Seleson, *J. Mechanics of Materials & Structures* (2014)

Peridynamic form of thermodynamics

- First law:

$$\dot{e} = \underline{\mathbf{T}} \bullet \underline{\dot{\mathbf{Y}}} + h + r$$

where e =internal energy density, h =energy transport rate, r =energy source rate.

- h is usually given by a nonlocal diffusion law such as

$$h(\mathbf{x}) = \int_{\mathcal{H}_x} k(\mathbf{q}, \mathbf{x})(\theta(\mathbf{q}) - \theta(\mathbf{x})) dV_{\mathbf{q}}$$

where k is a conductivity, θ =temperature.

- Second law:

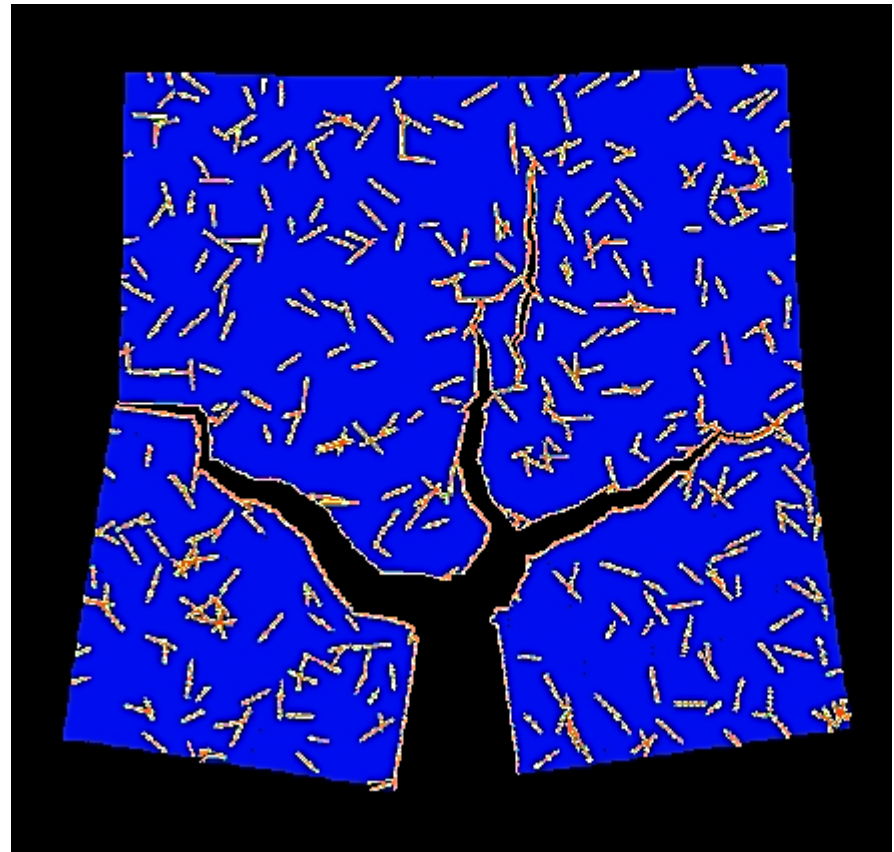
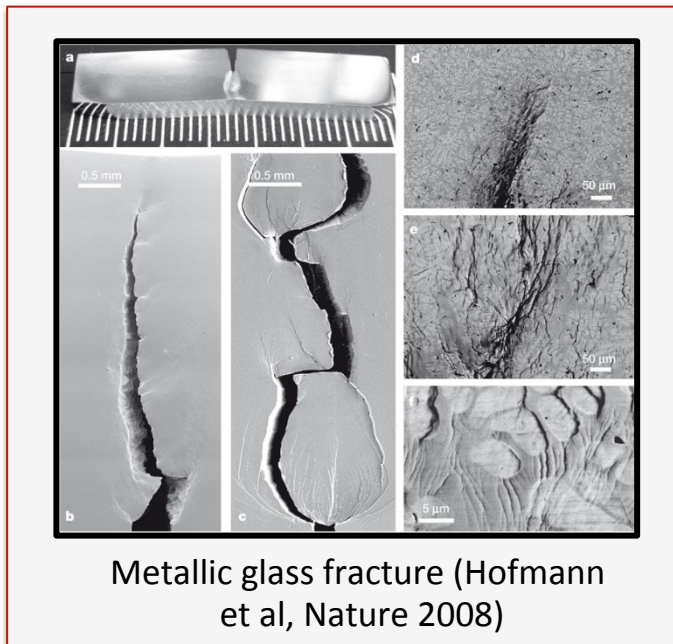
$$\theta \dot{\eta} \geq h + r$$

where η =entropy density.

- SS & Lehoucq, *Advances in Applied Mechanics* (2010)
- Bobaru, & Duangpanya, *J. Computational Physics* (2012)
- Oterkus, Madenci, & Agwai, *J. Mechanics & Physics of Solids* (2014)

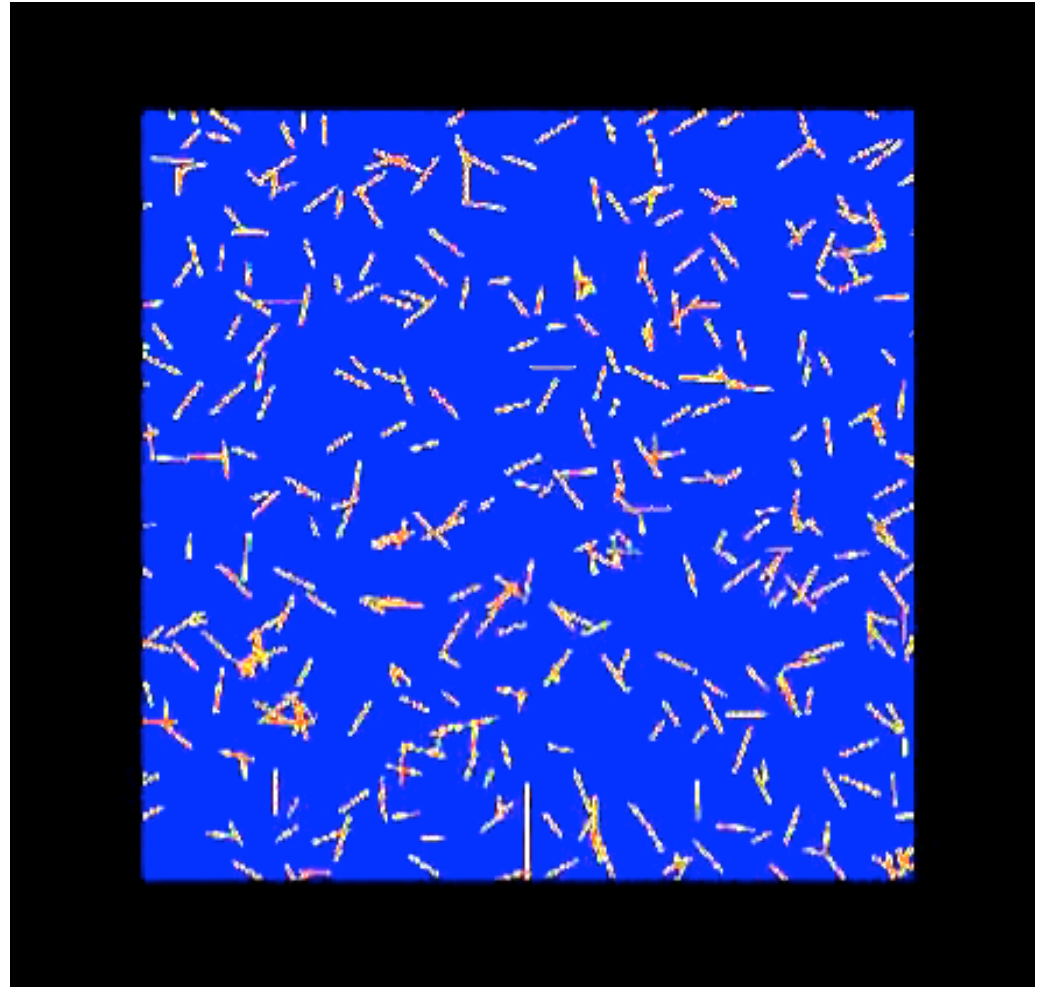
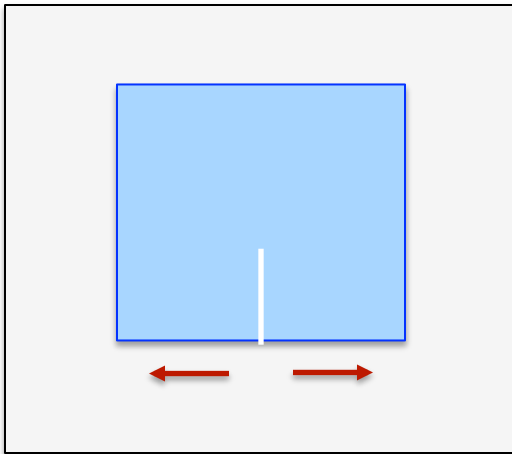
Fracture in a brittle plate with a lot of defects

- How do defects join up to form a macroscopic crack?



Fracture in a brittle plate with a lot of defects

VIDEO

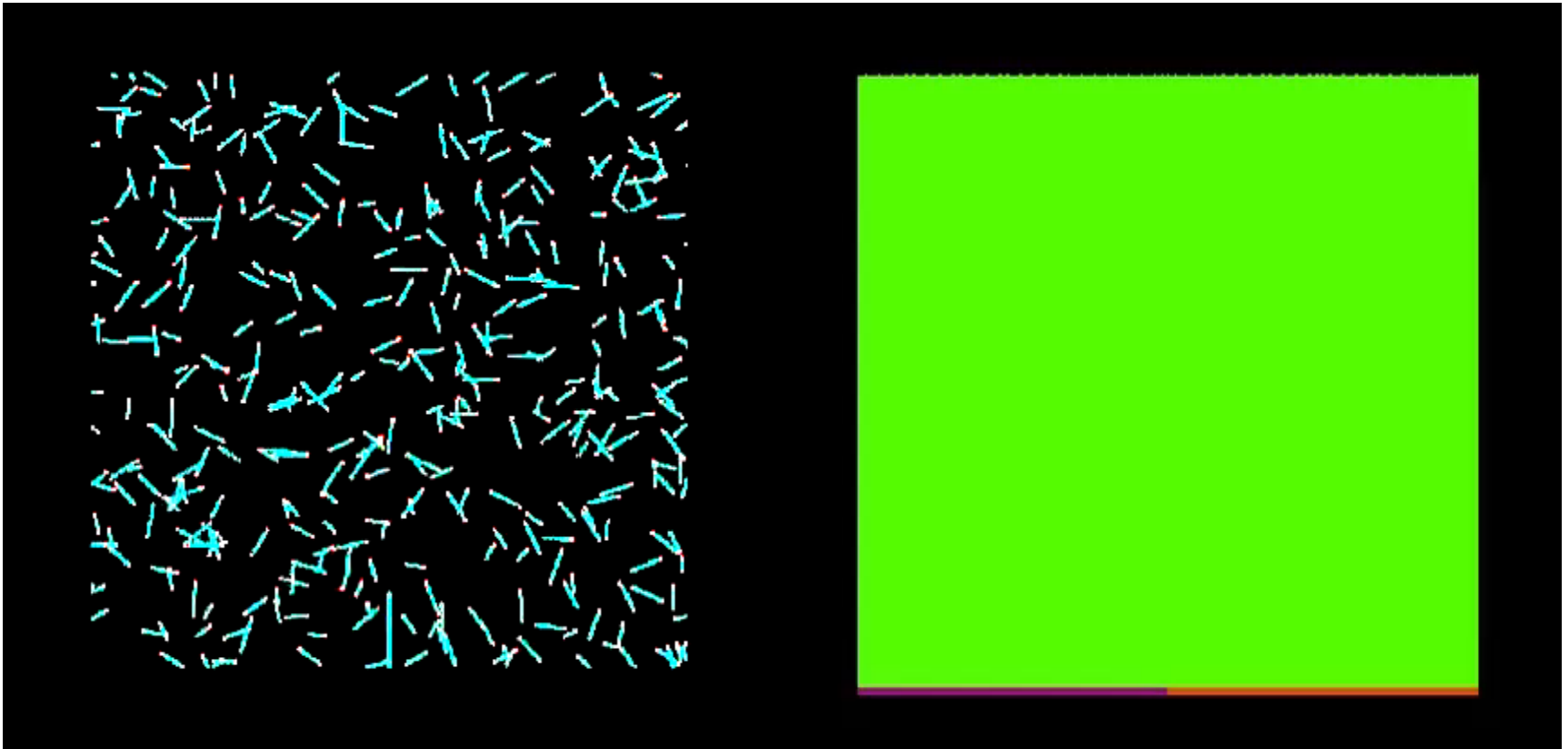


Fracture in an elastic-plastic plate with a lot of defects

VIDEOS

Defects

Displacement



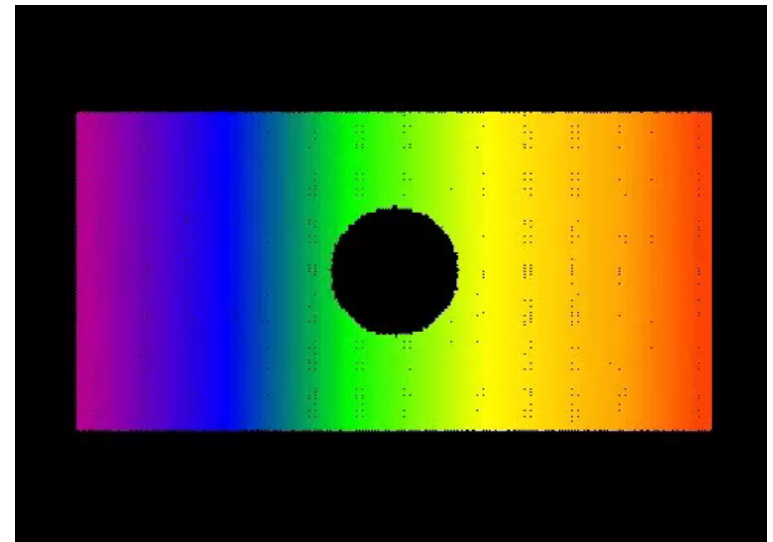
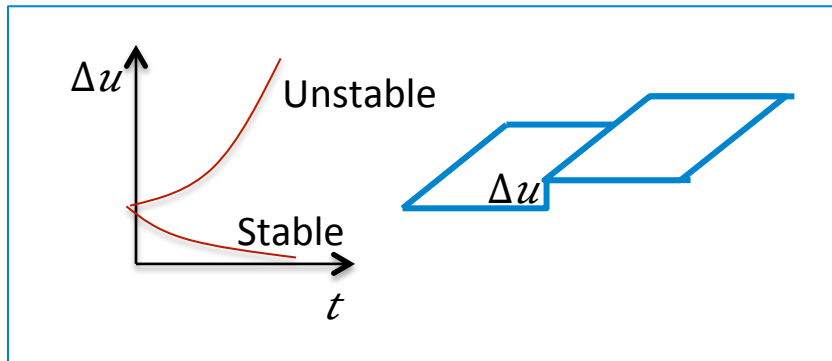
Cracks nucleate due to a material instability

- Condition for growth of a discontinuity in displacement:

$$\det(\underline{1} \bullet \underline{\mathbb{K}} \bullet \underline{1}) = 0$$

where $\underline{\mathbb{K}}$ is a tensor-valued state obtained from the second Fréchet derivatives of the strain energy density:

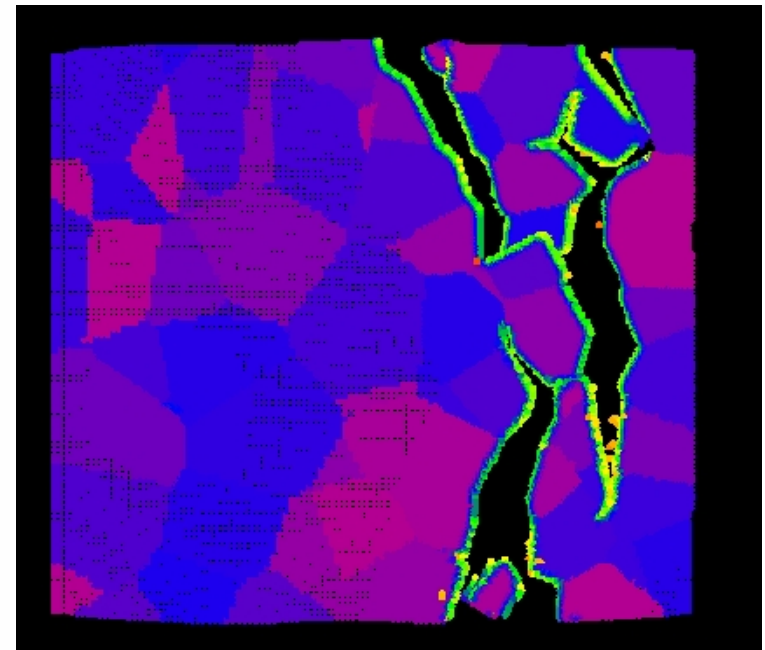
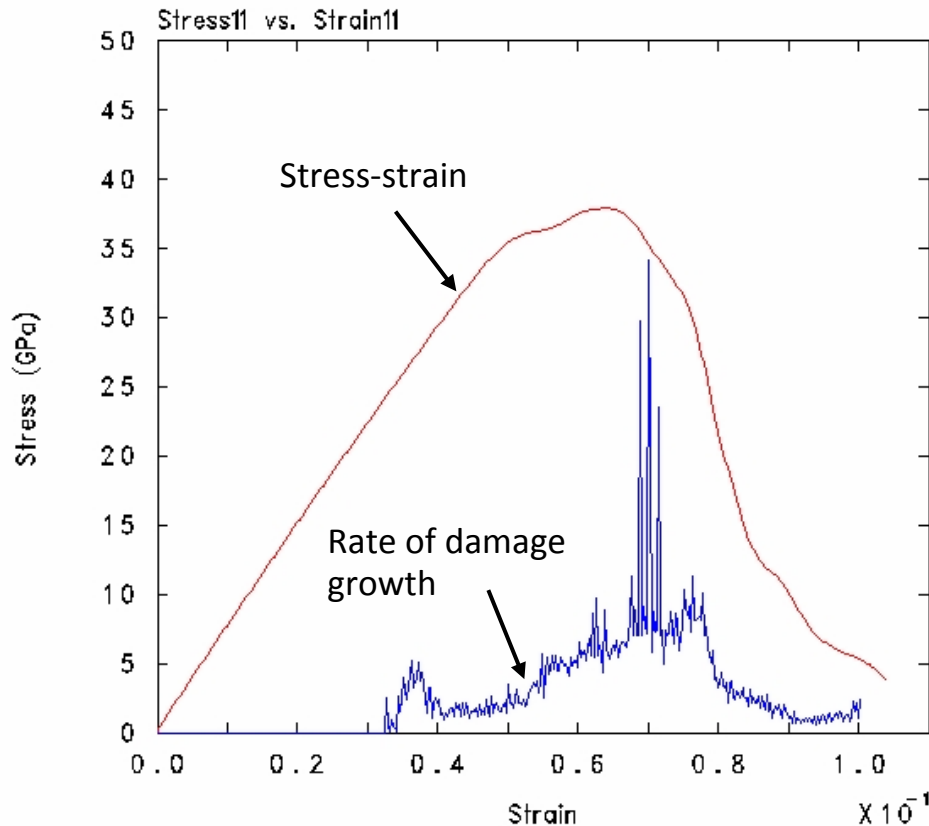
$$\underline{\mathbb{K}} = W_{\underline{\mathbf{Y}}\underline{\mathbf{Y}}}.$$



- SS, Weckner, Askari, & Bobaru, *Int. J. Fracture* (2010)
- Lipton, *J. Elast.* (2014)
- Lipton, *J. Elast.* (2015)

Multiscale model of a graphene sheet

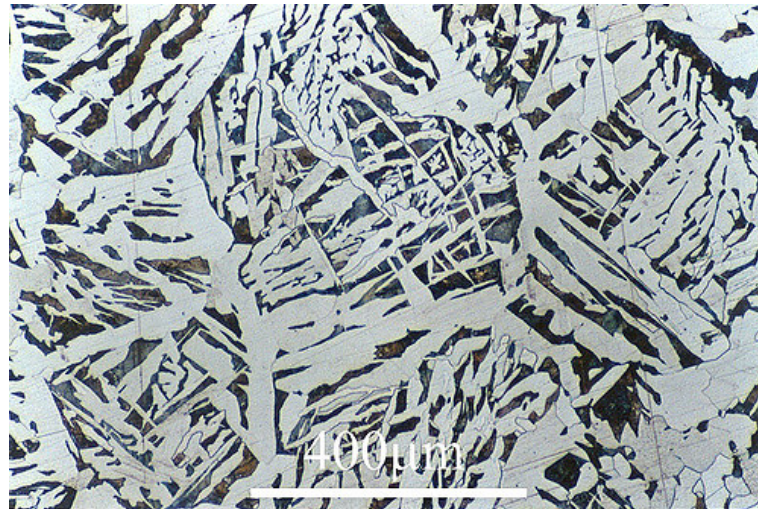
- Assign strength randomly to grain boundaries.
- This one realization fails at some stress under uniaxial tension.
- Repeating with more realizations leads to statistical distribution of strength of the polycrystal.



Cracks are mostly along grain boundaries

Microstructure

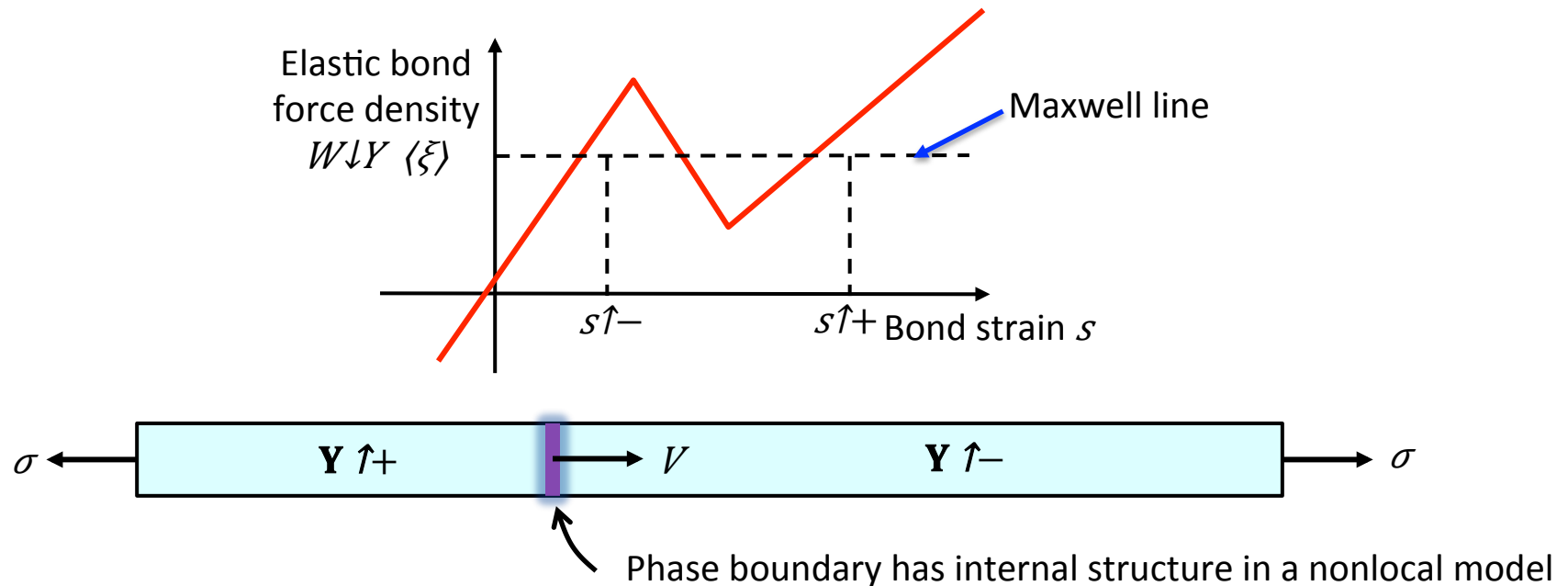
- Properties of metals are strongly influenced by their microstructure (sizes and shapes of grains).
- Microstructure evolution is largely about the energetics of grain boundaries.
- Will demonstrate:
 - Phase boundaries in peridynamics contain finite energy.
 - They dissipate energy as they move.
 - They move in the direction of lower total potential energy of the system.



Steel microstructure

Image: R F Cochrane, University of Leeds

Bond-based model for coexistent phases*

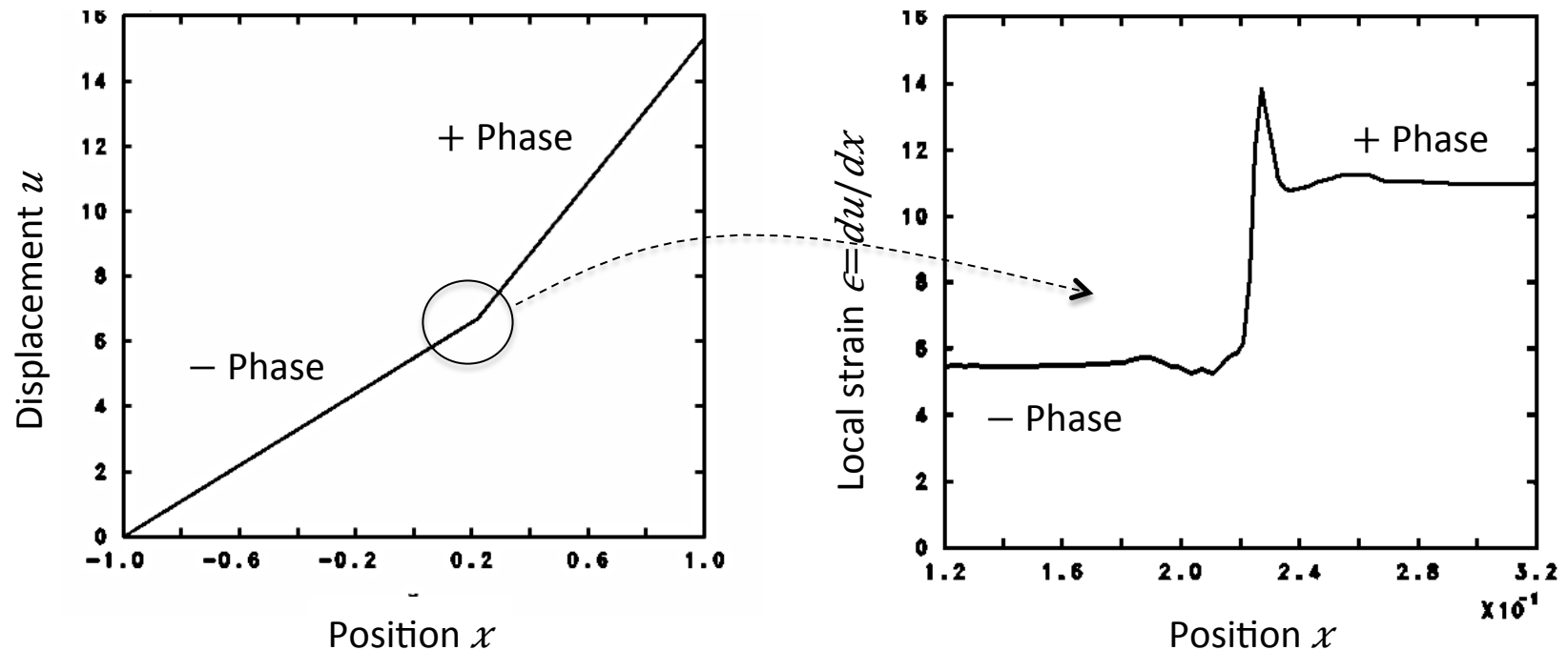


*Dayal & Bhattacharya, *J. Mechanics & Physics of Solids* (2006)

- Elastic bars: Ericksen, *J. Elast.* (1975)
- Crystals: James, *Archive for Rational Mechanics & Analysis* (1981)
- Strings: Purohit & Bhattacharya, *J. Mechanics & Physics of Solids* (2003)
- Lattices: Truskinovsky & Vainchtein, *SIAM J. Applied Math.* (2005)
- Inelastic continuum: Levitas, *Int. J. Solids & Structures* (1998)
- 3D elasticity: Abeyaratne & Knowles, *Archive for Rational Mechanics & Analysis* (1991)

Structure of the phase boundary in a peridynamic model

- Hard load problem in a bar.
- The phase boundary contains internal structure, finite width and energy.



- Dayal & Bhattacharya, *J. Mechanics & Physics of Solids* (2006)..

Condition for nucleation of a phase boundary

- Momentum balance across the phase boundary:

$$\left(\int_{\mathcal{H}} \Delta \underline{\mathbf{T}} \langle \underline{\boldsymbol{\xi}} \rangle \otimes \underline{\boldsymbol{\xi}} dV_{\underline{\boldsymbol{\xi}}} \right) \mathbf{n} = 0 \quad \text{or} \quad (\Delta \underline{\mathbf{T}} \star \underline{\mathbf{X}}) \mathbf{n} = 0.$$

- Continuity of displacement in the plane of the phase boundary:

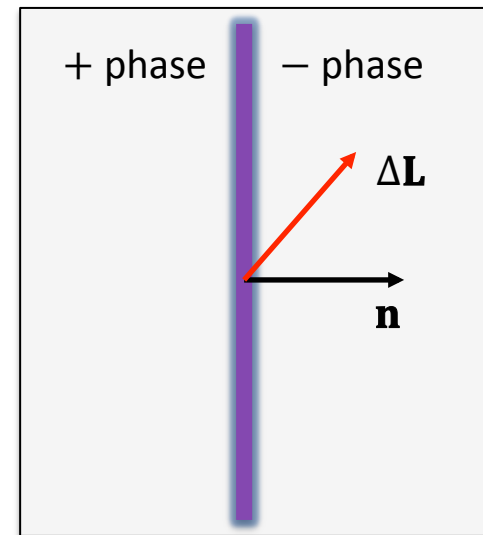
$$\Delta \underline{\mathbf{U}} = (\mathbf{n} \otimes \Delta \underline{\mathbf{L}}) \underline{\mathbf{X}} \quad \text{for some vector } \Delta \underline{\mathbf{L}} \neq 0.$$

- Linear material model: $\underline{\mathbf{T}} = \underline{\mathbb{K}} \bullet \underline{\mathbf{U}}$.
- The above lead to the following condition:

$$[\mathbb{C}(\mathbf{n} \otimes \mathbf{n})] \Delta \underline{\mathbf{L}} = 0.$$

where \mathbb{C} is the fourth order elasticity tensor, $\mathbb{C} = \underline{\mathbf{X}} \bullet (\underline{\mathbb{K}} \bullet \underline{\mathbf{X}})$.

- This condition holds if and only if $\det[\mathbb{C}(\mathbf{n} \otimes \mathbf{n})] = 0$. This is formally the same as loss of *ordinary ellipticity* in the local theory.



Condition for energy minimization with multiple phases

- Stationary potential energy for 2-phase equilibrium implies

$$\mathbf{n} \cdot (\Delta \mathbf{P} \mathbf{n}) = 0 \quad (1)$$

where \mathbf{P} is the Eshelby energy-momentum tensor, defined by

$$\mathbf{P} = W \mathbf{1} - \underline{\mathbf{T}} \star \underline{\mathbf{Y}} \quad \text{or} \quad \mathbf{P} = W \mathbf{1} - \int_{\mathcal{H}} \underline{\mathbf{T}} \langle \xi \rangle \otimes \underline{\mathbf{Y}} \langle \xi \rangle dV_{\xi}.$$

- (Compare classical version: $\mathbf{P} = W \mathbf{1} - \sigma \mathbf{F}^T$.)
- (1) leads to

$$\Delta \{ W - (\underline{\mathbf{T}} \cdot \mathbf{n}) \bullet (\underline{\mathbf{Y}} \cdot \mathbf{n}) \} = 0$$

which is the 3D peridynamic version of the 1D Maxwell condition for phase equilibrium

$$\Delta W - \sigma \Delta \epsilon = 0.$$

Energy dissipation model for a bond

- A moving phase boundary must dissipate energy.
- Introduce a dissipative term into the material model:

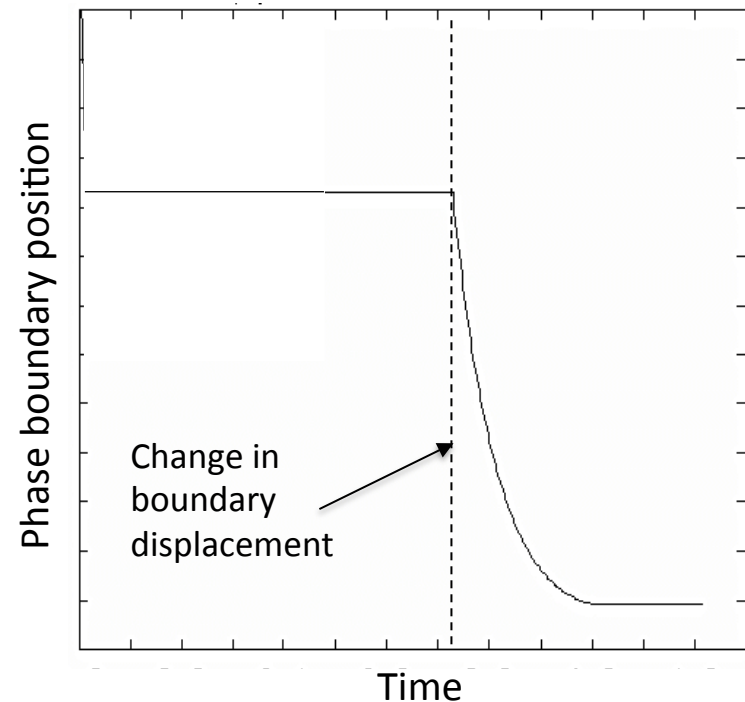
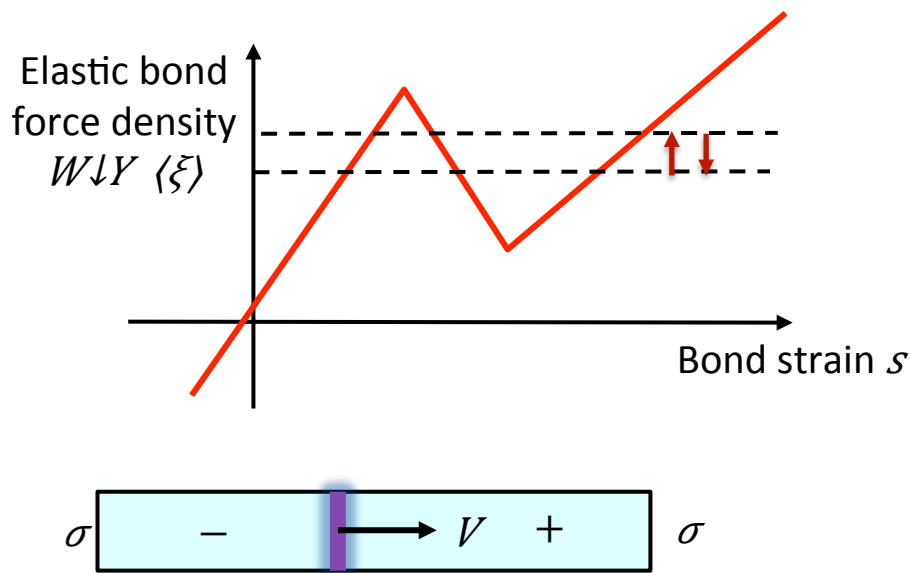
$$\begin{aligned}\underline{\mathbf{T}}\langle \xi \rangle &= W_{\underline{\mathbf{Y}}}\langle \xi \rangle + \gamma(\dot{\underline{\mathbf{Y}}}\langle \xi \rangle + \dot{\underline{\mathbf{Y}}}\langle -\xi \rangle) \\ &= W_{\underline{\mathbf{Y}}}\langle \xi \rangle + \gamma(\dot{\mathbf{y}}(\mathbf{x} + \xi) - 2\dot{\mathbf{y}}(\mathbf{x}) + \dot{\mathbf{y}}(\mathbf{x} - \xi)),\end{aligned}$$

where $\gamma > 0$ is a constant.

- Can show the new term satisfies the dissipation inequality.
 - Observe the dependence on the “curvature” of the velocity field – expect it to be significant only *within* a phase boundary.
-
- Abeyaratne & Knowles, *Archive for Rational Mechanics & Analysis* (1991).

Phase boundary seeks out the Maxwell line asymptotically

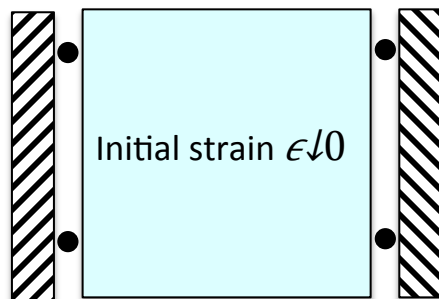
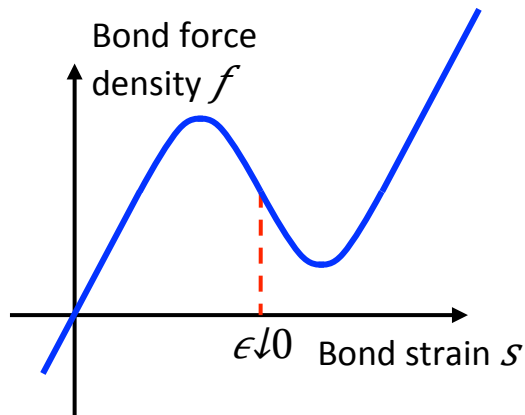
- Peridynamic simulation of a bar using the dissipation model discussed above.
- Perturb the boundary conditions and watch the phase boundary motion.
- The phase boundary moves so the system lowers its energy.



Deformation gradually reduces the area of a phase boundary in 2D

- Plate with ends fixed. Global strain $\epsilon \ll 0$ is in the unstable part of the material model.
- Complex microstructure appears at first, then simplifies.
- Driving force is the energy stuck in a phase boundary.

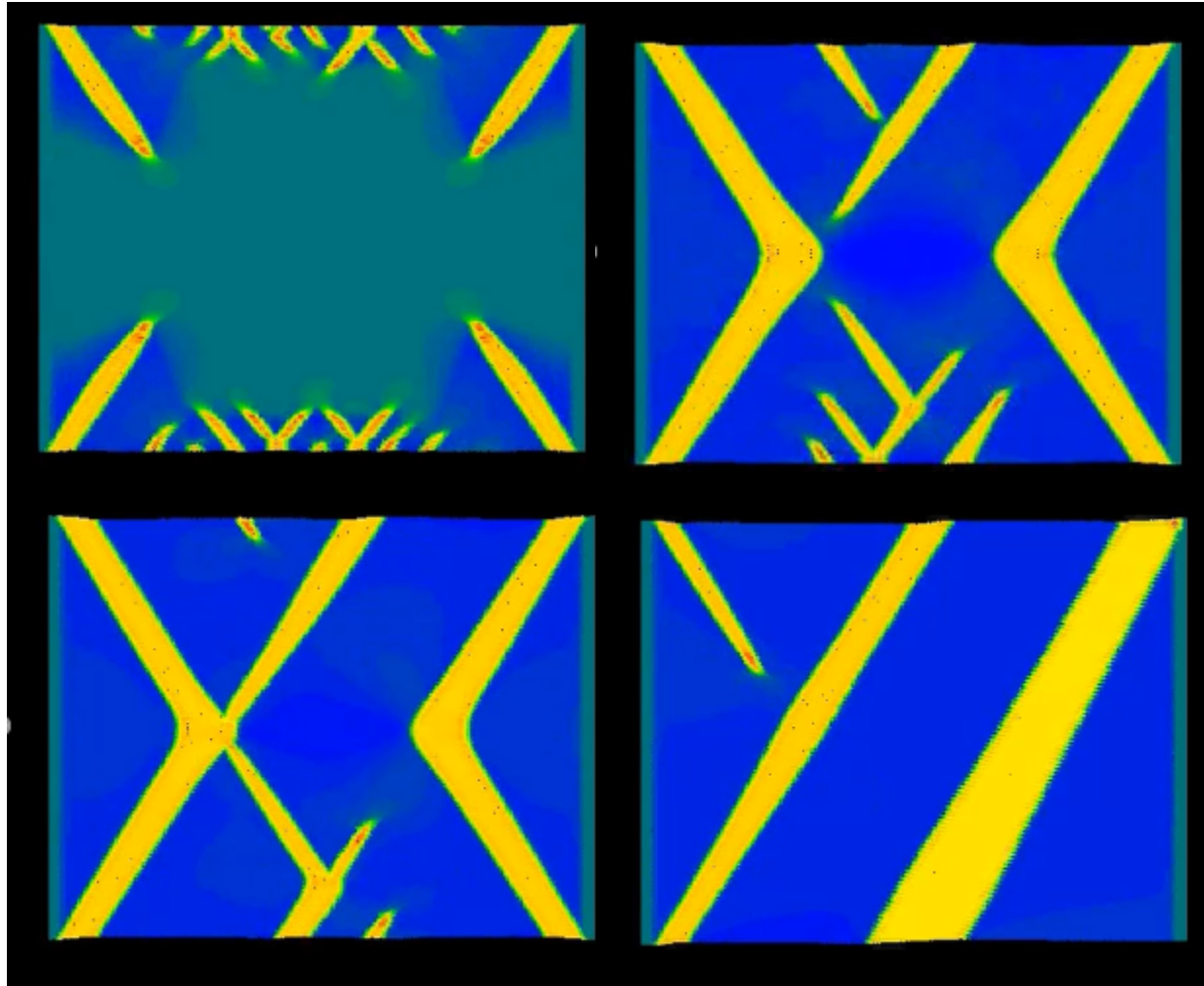
VIDEO



Colors show bond strain

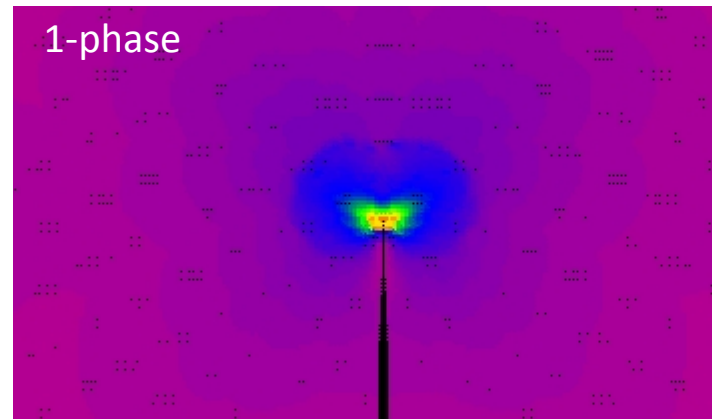
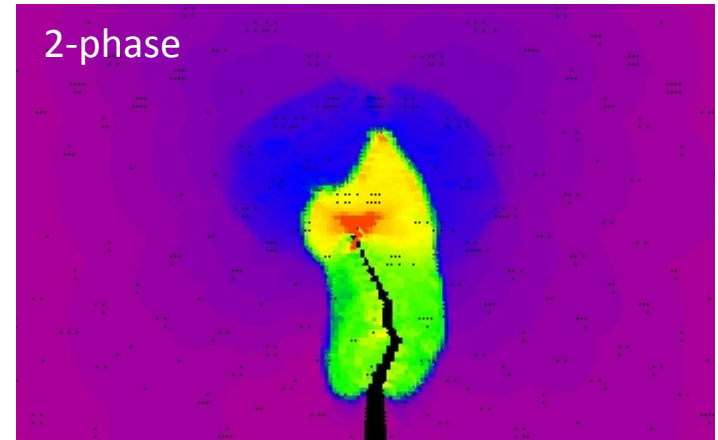
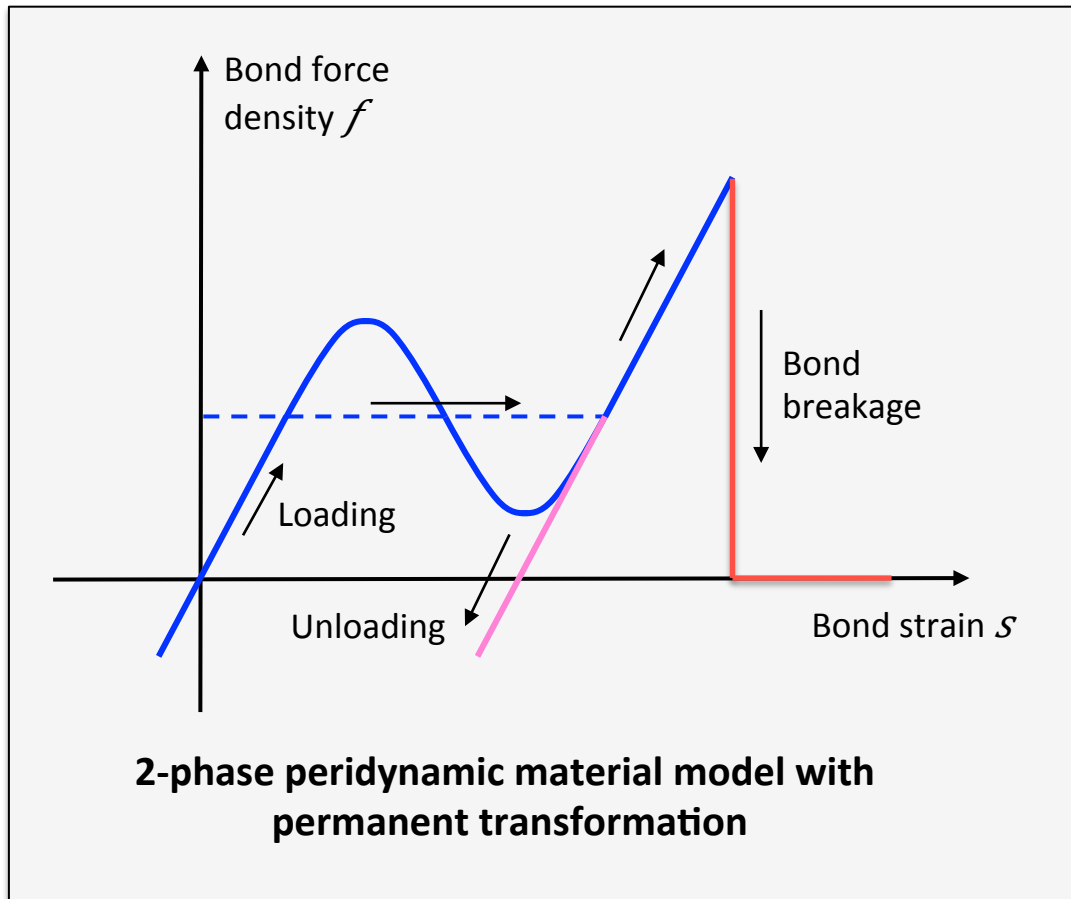
Deformation gradually reduces the area of a phase boundary in 2D

Colors show bond strain



Transformation toughening (isothermal)

- Can a phase transformation make a crack try to stay closed?
- Permanent transformation in each bond.

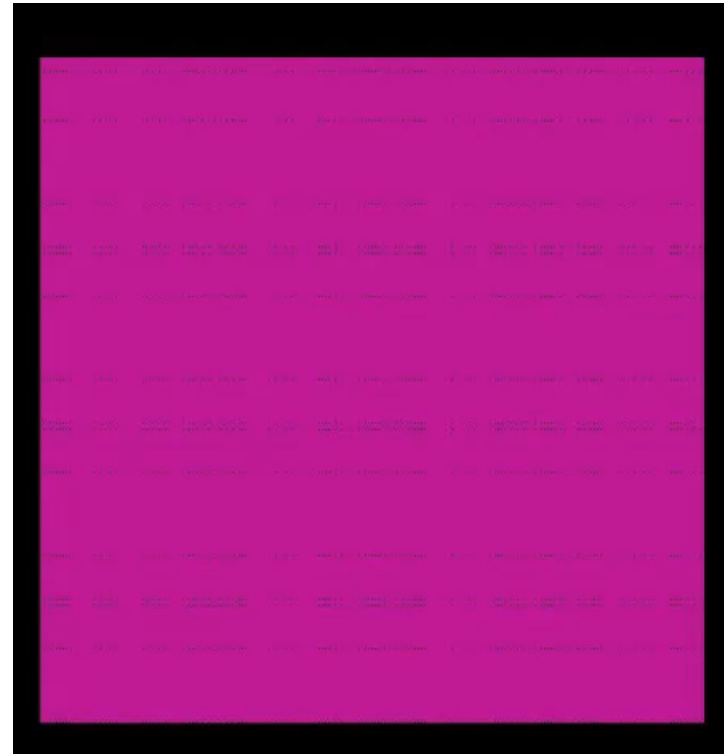
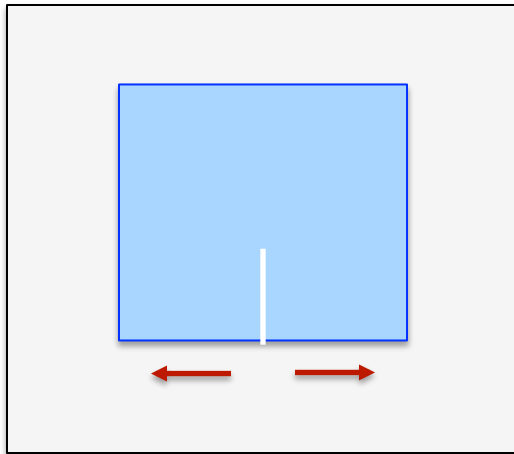


Colors show bond strain

Transformation toughening, ctd.

- Crack path deviates to avoid the toughened material in front of it.

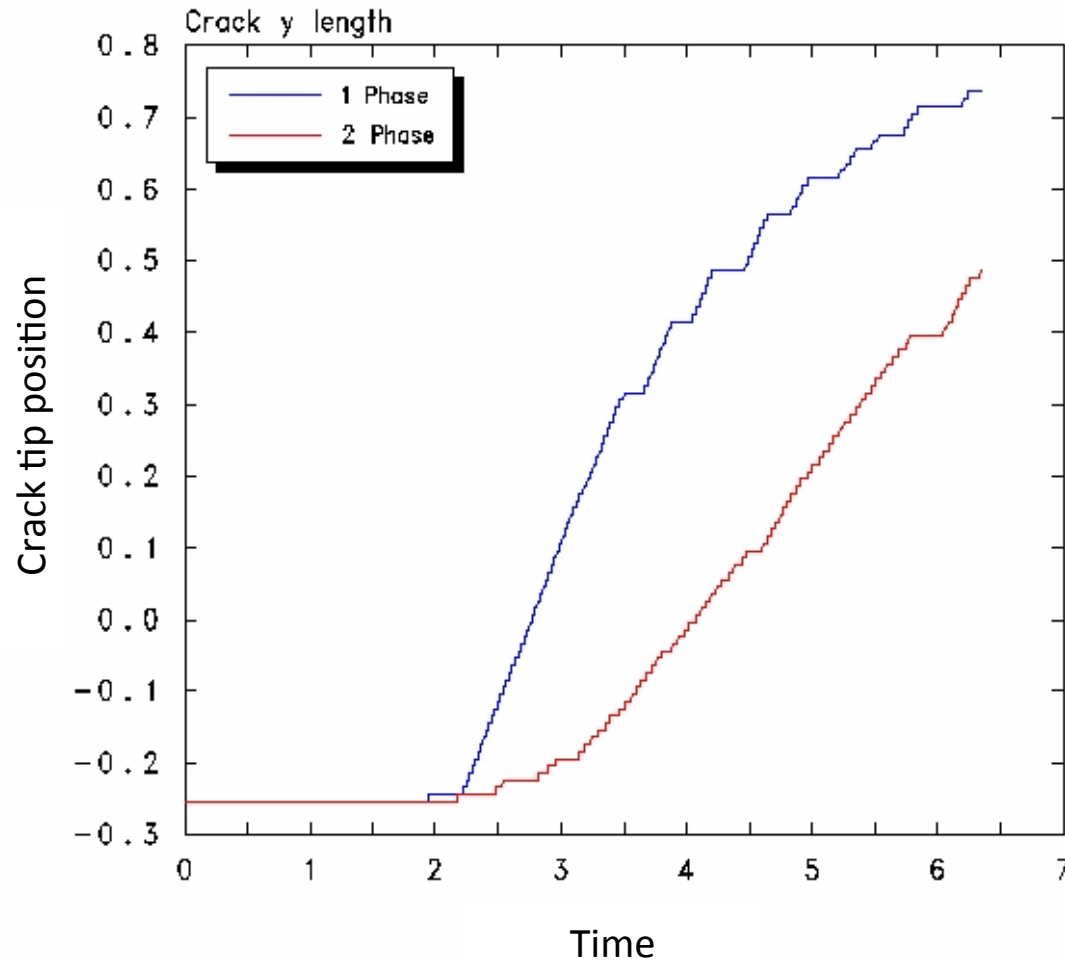
VIDEO



Colors show bond strain

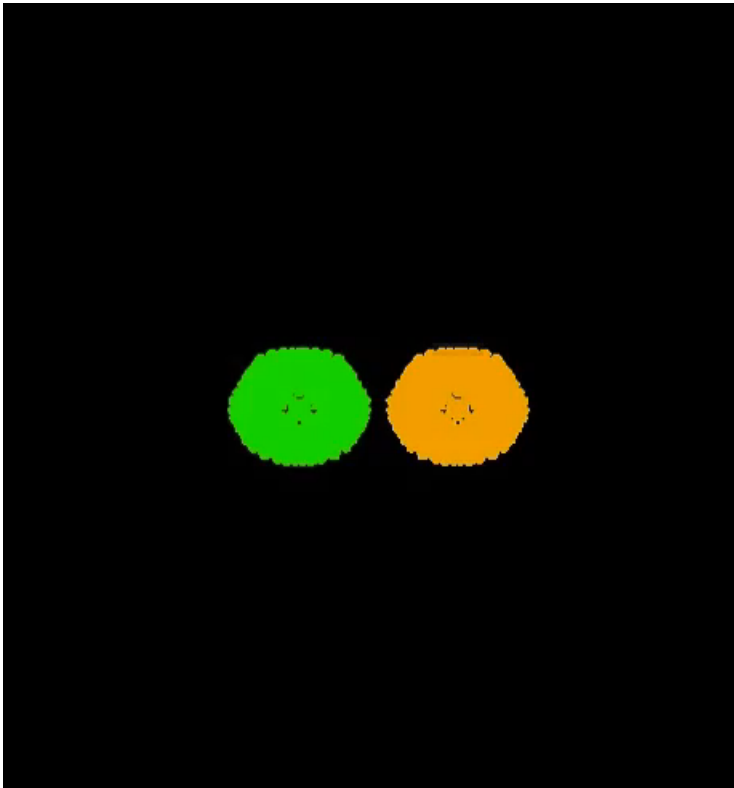
Transformation toughening, ctd.

- Crack grows slower in the 2-phase material.

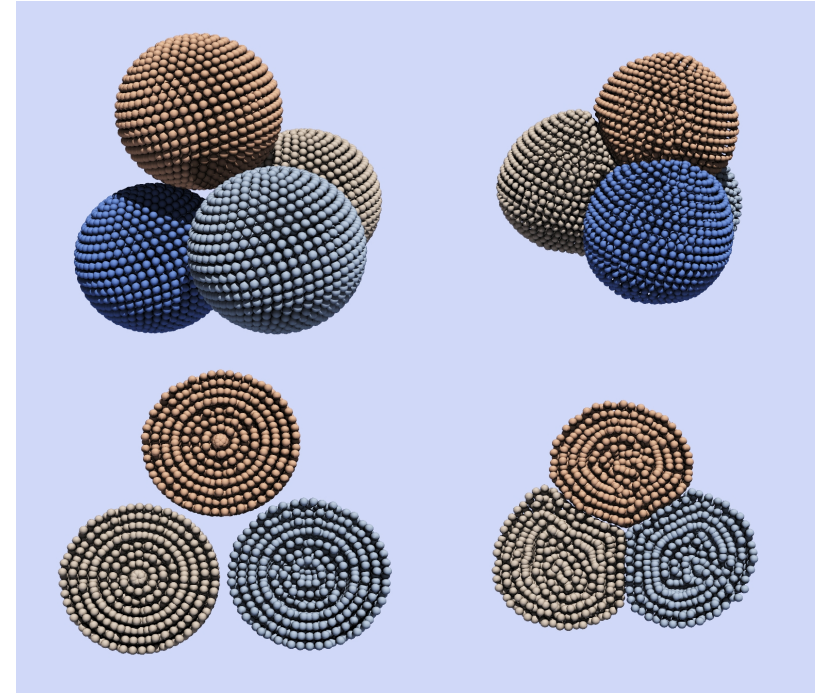


Free surfaces and material boundaries can have energy too

VIDEO



Droplet motion driven by surface tension



Sintering of 4 copper grains

Summary

- By treating discontinuous and continuous deformation within the same field equations we gain a lot in modeling some aspects of materials science.
 - Autonomous nucleation and growth of defects.
 - Phase boundaries evolve according to driving force.
 - Defects “do what they want.”
 - We avoid the need for supplemental equations that govern defect evolution.