

A two-phase flow model for a soft poroelastic drop in linear flows

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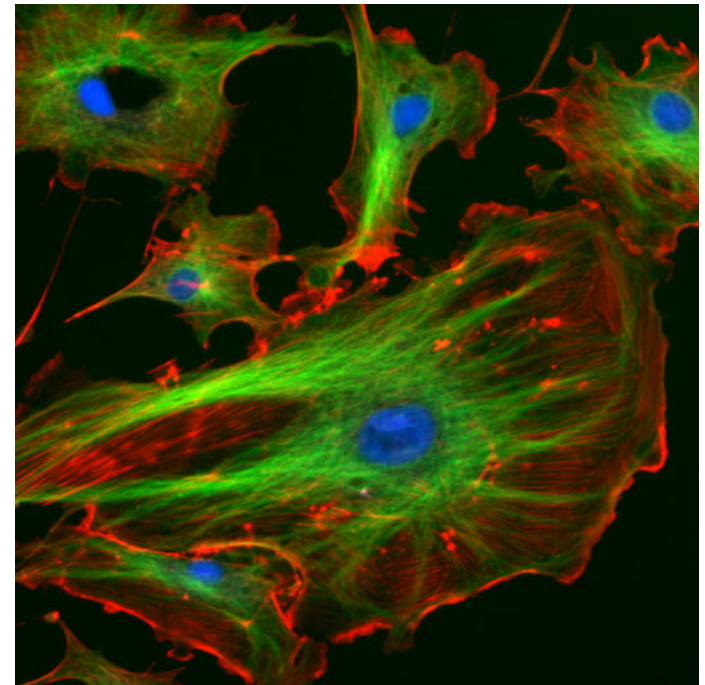
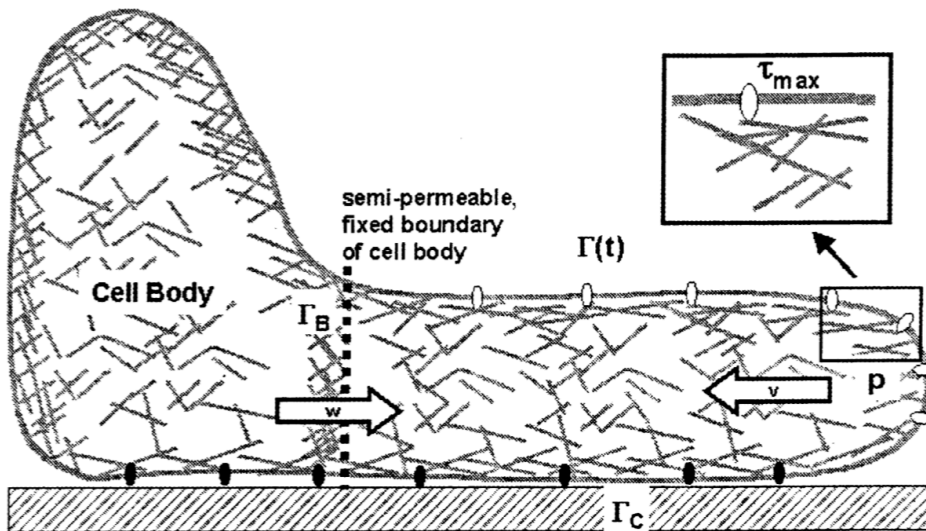
Yoichiro Mori, University of Minnesota

Michael Miksis, Northwestern University

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Motivation: cytoplasm consists of a viscous fluid, (monomers of) elastic fibers, and everything else (other than the nucleus)

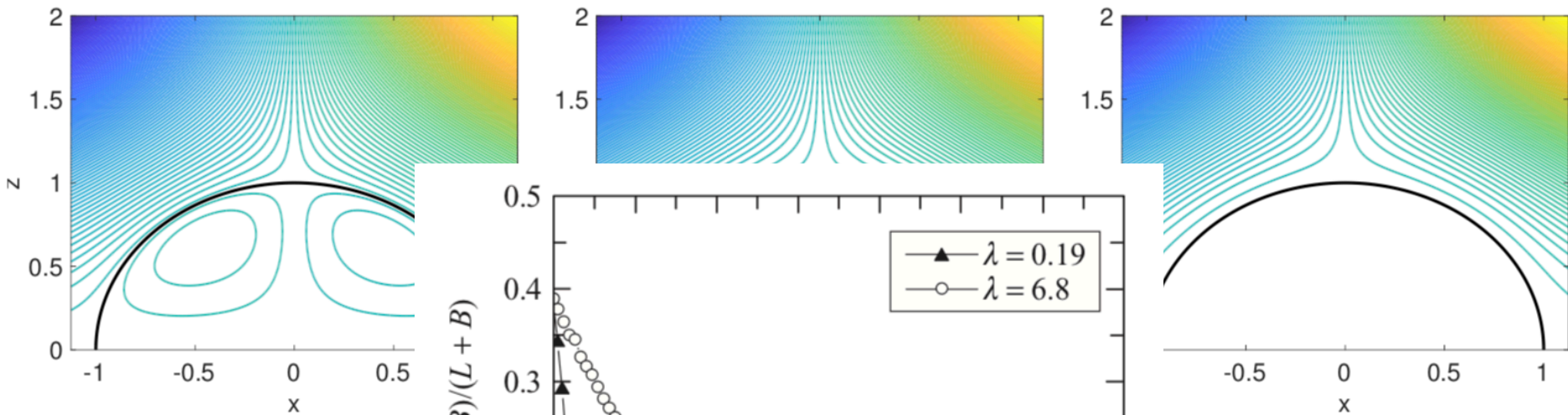


- Alt and Dembo, Math. Biosci. (1999)
- Strychalski *et al*, JCP (2014).

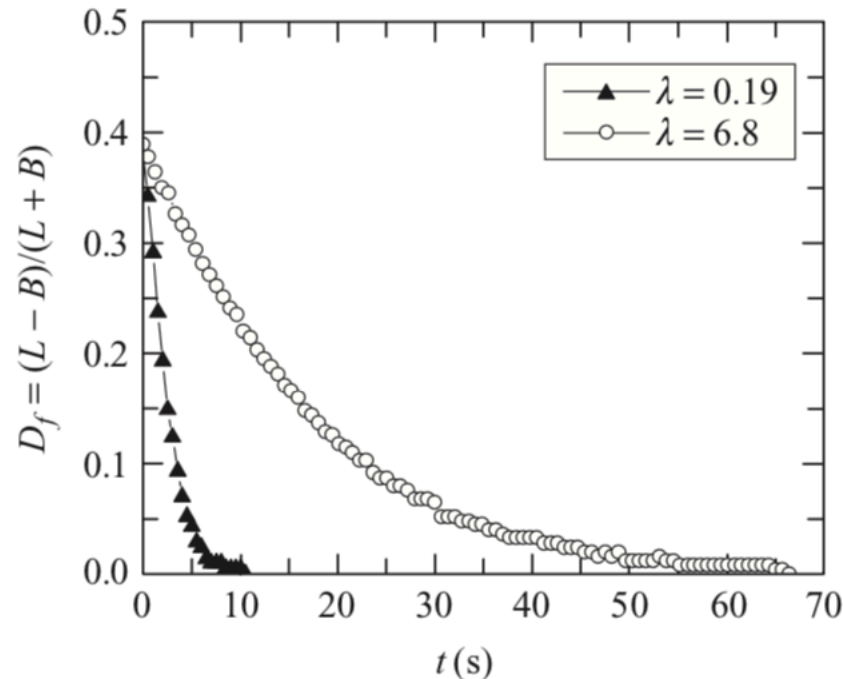
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outline

- Modeling cytoplasm as a viscous fluid filling a deformable elastic network -> a poroelastic



- Small-def
drop in pl



poroelastic

Mathematical modeling of cytoplasm:

Two-phase flow model for a network (s) phase in a viscous fluid (f)

- Cogan and Keener (Math. Med. and Biol., 2004)

$$\nabla \cdot (\phi_f \mu_f (\nabla \mathbf{u}_f + (\nabla \mathbf{u}_f)^T)) - \phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\phi_f + \phi_s = 1, \quad \frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0, \quad \nabla \cdot (\phi_s \mathbf{u}_s + \phi_f \mathbf{u}_f) = 0,$$

$\sigma_v = \mu_s (\nabla \mathbf{u}_s + (\nabla \mathbf{u}_s)^T)$ elastic stress σ_e neglected in this work

Mathematical modeling of cytoplasm:

Two-phase flow model for a network (s) phase in a viscous fluid (f)

- Mori *et al.* (SIAM J. Applied Math., 2013)

$$\nabla \cdot (\phi_f \mu_i (\nabla \mathbf{u}_f + (\nabla \mathbf{u}_f)^T)) - \phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\phi_f + \phi_s = 1, \quad \frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0, \quad \nabla \cdot (\phi_s \mathbf{u}_s + \phi_f \mathbf{u}_f) = 0,$$

$$\sigma_v = \mu_s (\nabla \mathbf{u}_s + (\nabla \mathbf{u}_s)^T) \quad \sigma_e = \phi_s \frac{\partial W_{elastic}(F)}{\partial F} F^T,$$

- This work also considers the polyelectrolytic solutions in the formulation.

Boundary conditions in Mori *et al.*

(SIAM J. Applied Math., 2013)

- Different from those in Cogan and Keener

$$(\mathbf{U} - \mathbf{u}_s) \cdot \mathbf{n} = \phi_f (\mathbf{u}_f - \mathbf{u}_s) \cdot \mathbf{n} \equiv w,$$

$$(\mathbf{U} - \mathbf{u}_s) \cdot (\mathbf{I} - \mathbf{nn}) = (\mathbf{u}_f - \mathbf{u}_s) \cdot (\mathbf{I} - \mathbf{nn}) \equiv \bar{\mathbf{q}},$$

$$\Sigma \cdot \mathbf{n} - (\sigma_f + \sigma_s) \cdot \mathbf{n} + [p]\mathbf{n} = 0,$$

- More boundary conditions needed

$$\eta_{\perp} w = \Pi_{\perp} = \mathbf{n} \cdot \Sigma \cdot \mathbf{n} - \mathbf{n} \cdot \left(\frac{\sigma_f}{\phi_f} \right) \cdot \mathbf{n} + [p],$$

$$\eta_{\parallel} \bar{\mathbf{q}} = \Pi_{\parallel} = (\sigma_s \cdot \mathbf{n})_{\parallel},$$

- MacMinn *et al.* (Phys. Rev. Appl., 2016)

$$-\phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \nabla p \equiv \nabla \cdot (\phi_s \sigma') - \nabla p = 0,$$

$$\phi_f + \phi_s = 1, \quad \frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0, \quad \nabla \cdot (\phi_s \mathbf{u}_s + \phi_f \mathbf{u}_f) = 0,$$

$$\text{viscous dissipation } \sigma_v = 0, \quad \sigma' = \sigma_e = \Lambda \text{tr}(\mathbf{H}) \mathbf{I} + (M - \Lambda) \mathbf{H},$$

$$\mathbf{H} = \frac{1}{2} \ln(\mathbf{F}\mathbf{F}^T), \quad \mathbf{F}^{-1} = \mathbf{I} - \nabla \mathbf{v}_s,$$

$$\mathbf{u}_s = \mathbf{q} - \frac{\phi_f}{\xi \phi_s} \nabla p, \quad \mathbf{u}_f = \mathbf{q} + \frac{1}{\xi} \nabla p,$$

Small-deformation and linear poroelasticity

- Small deformation: $\frac{\phi_f - \phi_{f,0}}{1 - \phi_{f,0}} \approx \nabla \cdot \mathbf{v}_s \ll 1,$

- Linear poroelasticity:

$$\sigma' = \Lambda \text{tr}(\varepsilon) + (M - \Lambda) \varepsilon, \quad \text{with } \varepsilon \equiv \frac{1}{2} \left[\nabla \mathbf{v}_s + (\nabla \mathbf{v}_s)^T \right],$$

- Coupled to an external Stokes flow:

$$\mu_e \nabla^2 \mathbf{U} - \nabla P = 0, \quad \nabla \mathbf{U} = 0,$$

Summary of two-phase flow model

- Conservation of mass:

$$\phi_f + \phi_s = 1, \quad \frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0, \quad \nabla \cdot (\phi_s \mathbf{u}_s + \phi_f \mathbf{u}_f) = 0,$$

- Momentum balance:

$$\nabla \cdot (\phi_f \mathbf{e}_f) - \phi_f \nabla p + \mathcal{N}^{s \rightarrow f} + \phi_f \rho_f \mathbf{g} = 0, \quad \mathcal{N}^{s \rightarrow f} \equiv -\xi \phi_f \phi_s (\mathbf{u}_f - \mathbf{u}_s),$$

$$\nabla \cdot (\phi_s \mathbf{e}_s) - \phi_s \nabla p + \mathcal{N}^{f \rightarrow s} + \phi_s \rho_s \mathbf{g} = 0, \quad \mathcal{N}^{f \rightarrow s} \equiv -\mathcal{N}^{s \rightarrow f} = \xi \phi_f \phi_s (\mathbf{u}_f - \mathbf{u}_s),$$

- Incompressible Darcy equations are derived as a limit of dominant solid stress over fluid stress.

$$-\phi_f \nabla p - \xi \phi_f \phi_s (\mathbf{u}_f - \mathbf{u}_s) = -\rho \mathbf{g} \text{ when } \sigma' = \phi_f \mathbf{e}_f + \phi_s \mathbf{e}_s \approx \phi_s \mathbf{e}_s,$$

- Solid structure is allowed to deform (soft solid), and the usual Darcy equations are obtained when the strain is fixed in time ($\mathbf{u}_s=0$).

Summary of two-phase model (cont.)

- Exterior Stokesian fluid

$$\nabla \cdot (\mu_e \mathbf{E}) - \nabla P = \mu_e \nabla^2 \mathbf{U} - \nabla P = 0,$$

$$\nabla \cdot \mathbf{U} = 0,$$

- Interior poroelastic Brinkman fluid

$$\nabla \cdot (\phi_f \mu_i \mathbf{e}_f) - \phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0,$$

$$\phi_f + \phi_s = 1, \quad \nabla \cdot (\phi_f \mathbf{u}_f + \phi_s \mathbf{u}_s) = 0.$$

- Interior poroelastic Darcy fluid

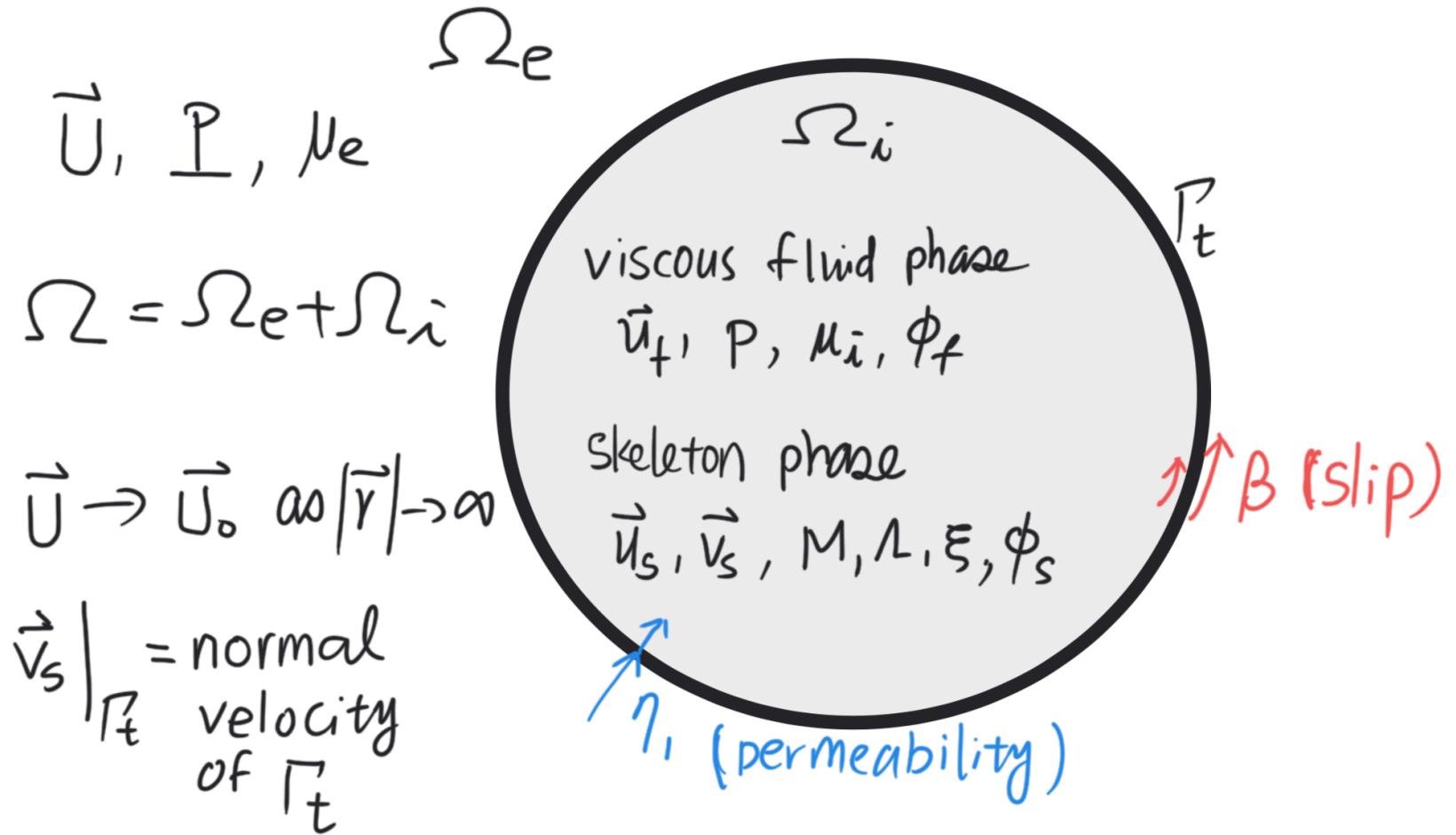
$$-\phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0,$$

$$\phi_f + \phi_s = 1, \quad \nabla \cdot (\phi_f \mathbf{u}_f + \phi_s \mathbf{u}_s) = 0.$$

Boundary conditions: a simple derivation



Boundary conditions: a simple derivation

$$\begin{aligned}
 & \int_{\Omega} \mathbf{U} \cdot [\nabla(\mu_e \mathbf{E}) - \nabla P] d^3x \\
 & + \int_{\Omega} \mathbf{u}_f \cdot [\nabla(\phi_f \mu_i \mathbf{e}_f) - \phi_f \nabla p - \xi \phi_f \phi_s (\mathbf{u}_f - \mathbf{u}_s)] d^3x \\
 & + \int_{\Omega} \mathbf{u}_s \cdot [\nabla \cdot (\phi_s \sigma_s) - \phi_s \nabla p + \xi \phi_f \phi_s (\mathbf{u}_f - \mathbf{u}_s)] d^3x \\
 & = \int_{\Gamma_t} -\mathbf{U} \cdot (\mu_e \mathbf{E} - P \mathbf{I}) \cdot \hat{\mathbf{n}} ds - \int_{\Omega} \mu_e \mathbf{E} : \nabla \mathbf{U} d^3x \\
 & + \int_{\Gamma_t} \mathbf{u}_f \cdot (\phi_f \mu_i \mathbf{e}_f - \phi_f p \mathbf{I}) \hat{\mathbf{n}} ds - \int_{\Omega} \phi_f \mu_i \mathbf{e}_f : \nabla \mathbf{u}_f d^3x \\
 & + \int_{\Gamma_t} \mathbf{u}_s \cdot (\phi_s \sigma_s - \phi_s p \mathbf{I}) \hat{\mathbf{n}} ds - \int_{\Omega} \phi_s \sigma_s : \nabla \mathbf{u}_s d^3x .
 \end{aligned}$$

- Velocities relative to the skeleton velocity: $\bar{\mathbf{U}} = \mathbf{U} - \mathbf{u}_s$, $\bar{\mathbf{u}}_f = \phi_f(\mathbf{u}_f - \mathbf{u}_s)$,
- Surface integrals after the integration by parts:

$$\begin{aligned} & \int_{\Gamma_t} -(\bar{\mathbf{U}} + \mathbf{u}_s)(\mu_e \mathbf{E} - P\mathbf{I})\hat{\mathbf{n}} + \left(\frac{\bar{\mathbf{u}}_f}{\phi_f} + \mathbf{u}_s\right)(\phi_f \mu_i \mathbf{e}_f - \phi_f p\mathbf{I})\hat{\mathbf{n}} + \mathbf{u}_s(\phi_s \sigma_s - \phi_s p\mathbf{I})\hat{\mathbf{n}} ds \\ &= \int_{\Gamma_t} \mathbf{u}_s \cdot (-\mu_e \mathbf{E} + P\mathbf{I} + \phi_f \mu_i \mathbf{e}_f + \phi_s \sigma_s - p\mathbf{I})\hat{\mathbf{n}} ds + \\ & \quad \int_{\Gamma_t} -\bar{\mathbf{U}} \cdot (\mu_e \mathbf{E} - P\mathbf{I})\hat{\mathbf{n}} + \bar{\mathbf{u}}_f \cdot (\mu_i \mathbf{e}_f - p\mathbf{I})\hat{\mathbf{n}} ds. \end{aligned}$$

- Decomposition: $\bar{\mathbf{U}} = \bar{\mathbf{U}}_{\perp} + \bar{\mathbf{U}}_{\parallel}$, $\bar{\mathbf{u}}_f = \bar{\mathbf{u}}_{f\perp} + \bar{\mathbf{u}}_{f\parallel}$
- Normal component: $\bar{\mathbf{U}}_{\perp} = \bar{\mathbf{u}}_{f\perp} \rightarrow (\mathbf{U} - \mathbf{u}_s) \cdot \hat{\mathbf{n}} = \phi_f (\mathbf{u}_f - \mathbf{u}_s) \cdot \hat{\mathbf{n}}$.

$$\bar{\mathbf{U}}_{\perp} = \bar{\mathbf{u}}_{f\perp} = \eta_1 \hat{\mathbf{n}} \cdot (\mu_e \mathbf{E} - P\mathbf{I} - \mu_i \mathbf{e}_f + p\mathbf{I}) \cdot \hat{\mathbf{n}}$$

Boundary conditions (cont.)

- Tangential component:

$$\bar{\mathbf{U}}_{\parallel} = \frac{\beta}{2} (\mu_e \mathbf{E} \cdot \hat{\mathbf{n}})_{\parallel} - \gamma (\mu_i \mathbf{e}_f \cdot \hat{\mathbf{n}})_{\parallel} = \frac{\beta}{2} (\mu_e \mathbf{E} \cdot \hat{\mathbf{n}})_{\parallel},$$
$$\bar{\mathbf{u}}_{f\parallel} = \alpha (\mu_e \mathbf{E} \cdot \hat{\mathbf{n}})_{\parallel} - \frac{\beta}{2} (\mu_i \mathbf{e}_f \cdot \hat{\mathbf{n}})_{\parallel} = -\frac{\beta}{2} (\mu_i \mathbf{e}_f \cdot \hat{\mathbf{n}})_{\parallel},$$

- Interior Darcy flow: Beavers-Joseph slip boundary condition is recovered (Beavers and Joseph, JFM, 1967)
- Interior Brinkman flow: Stokes-Brinkman slip boundary condition is recovered (Angot, Goyeau, and Ochoa-Tapia, PRE, 2017)
- Roughness of the Stokes-Brinkman (or Stokes-Darcy) boundary gives rise to small slip and permeability

Boundary conditions: summary

$$[(\mathbf{U} - \mathbf{u}_s) - \phi_f (\mathbf{u}_f - \mathbf{u}_s)] \cdot \hat{\mathbf{n}} = 0,$$

$$(\mathbf{U} - \mathbf{u}_s) \cdot \hat{\mathbf{n}} = \eta_1 \hat{\mathbf{n}} \cdot [(\mu_e \mathbf{E} - P\mathbf{I}) - (\mu_i \mathbf{e}_f - p\mathbf{I})] \cdot \hat{\mathbf{n}},$$

$$[(\mathbf{U} - \mathbf{u}_s)] \cdot \hat{\mathbf{t}} = \frac{\beta}{2} \hat{\mathbf{n}} \cdot \mu_e \mathbf{E} \cdot \hat{\mathbf{t}},$$

$$[\phi_f (\mathbf{u}_f - \mathbf{u}_s)] \cdot \hat{\mathbf{t}} = -\frac{\beta}{2} \hat{\mathbf{n}} \cdot \mu_i \mathbf{e}_f \cdot \hat{\mathbf{t}},$$

$$\hat{\mathbf{n}} \cdot [(\mu_e \mathbf{E} - P\mathbf{I}) - (\phi_s \sigma_s + \phi_f \mu_i \mathbf{e}_f - p\mathbf{I})] \cdot \hat{\mathbf{n}} = \kappa \gamma,$$

$$\hat{\mathbf{t}} \cdot [(\mu_e \mathbf{E} - P\mathbf{I}) - (\phi_s \sigma_s + \phi_f \mu_i \mathbf{e}_f - p\mathbf{I})] \cdot \hat{\mathbf{n}} = 0,$$

$$-\phi_f \nabla p - \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\nabla \cdot (\phi_s (\sigma_v + \sigma_e)) - \phi_s \nabla p + \xi \phi_s \phi_f (\mathbf{u}_f - \mathbf{u}_s) = 0,$$

$$\frac{\partial \phi_s}{\partial t} + \nabla \cdot (\phi_s \mathbf{u}_s) = 0,$$

$$\phi_f + \phi_s = 1, \quad \nabla \cdot (\phi_f \mathbf{u}_f + \phi_s \mathbf{u}_s) = 0.$$

A Darcy drop in a linear flow: small-deformation

$$r = 1 + \delta r(t, \theta) = 1 + \mathbf{v}_s \cdot \hat{\mathbf{r}}, \quad |\delta r| = |\mathbf{v}_s \cdot \hat{\mathbf{r}}| \ll 1.$$

$$\mathbf{u}_s = \frac{d\mathbf{v}_s}{dt} = \frac{\partial \mathbf{v}_s}{\partial t} + \mathbf{u}_s \cdot \nabla \mathbf{v}_s \approx \frac{\partial \mathbf{v}_s}{\partial t}$$

- Consequence of small-deformation

$$\frac{\partial \phi_f}{\partial t} + \nabla \cdot \left(\phi_f \frac{d\mathbf{v}_s}{dt} \right) = (1 - \phi_0) \frac{\partial}{\partial t} (\nabla \cdot \mathbf{v}_s) + \nabla \cdot \left(\phi_0 \frac{d\mathbf{v}_s}{dt} \right) + h.o.t.$$

$$0 \approx (1 - \phi_0) \left(\nabla \cdot \frac{\partial \mathbf{v}_s}{\partial t} \right) + \nabla \cdot \left(\phi_0 \frac{\partial \mathbf{v}_s}{\partial t} \right) + h.o.t.$$

$$\nabla \cdot \left(\frac{\partial \mathbf{v}_s}{\partial t} \right) \approx 0.$$

A Darcy drop in a linear flow: small-deformation

$$r = 1 + \delta r(t, \theta) = 1 + \mathbf{v}_s \cdot \hat{\mathbf{r}}, \quad |\delta r| = |\mathbf{v}_s \cdot \hat{\mathbf{r}}| \ll 1.$$

$$\mathbf{u}_s = \frac{d\mathbf{v}_s}{dt} = \frac{\partial \mathbf{v}_s}{\partial t} + \mathbf{u}_s \cdot \nabla \mathbf{v}_s \approx \frac{\partial \mathbf{v}_s}{\partial t}$$

$$-\phi_0 \nabla p - \xi \phi_0 (1 - \phi_0) \left(\mathbf{u}_f - \frac{\partial \mathbf{v}_s}{\partial t} \right) = 0,$$

$$\nabla \cdot ((1 - \phi_0) (\sigma_e(\mathbf{v}_s) + \alpha_v \sigma_v(\mathbf{u}_s))) - \nabla p = 0,$$

$$\nabla \cdot (\phi_0 \mathbf{u}_f + (1 - \phi_0) \mathbf{u}_s) = 0.$$

- Uniaxial extensional flow
- Planar shear flow

Small-deformation of a Darcy drop in a uniaxial extensional flow

$$\begin{pmatrix} \mathbf{u}_f \\ \mathbf{v}_s \\ p \end{pmatrix} = \begin{pmatrix} \mathbf{u}_{f,e} \\ \mathbf{v}_{s,e} \\ p_e \end{pmatrix} + e^{\lambda t} \begin{pmatrix} \mathbf{u}_{f,1} \\ \mathbf{v}_{s,1} \\ p_1 \end{pmatrix}$$

$$p_e = -\frac{21}{10}(1 - \phi_0)(1 - \Lambda)d_1r^2 (1 + 3 \cos(2\theta)),$$

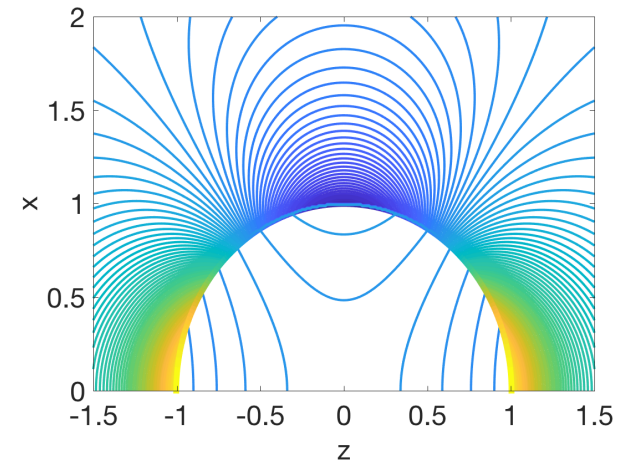
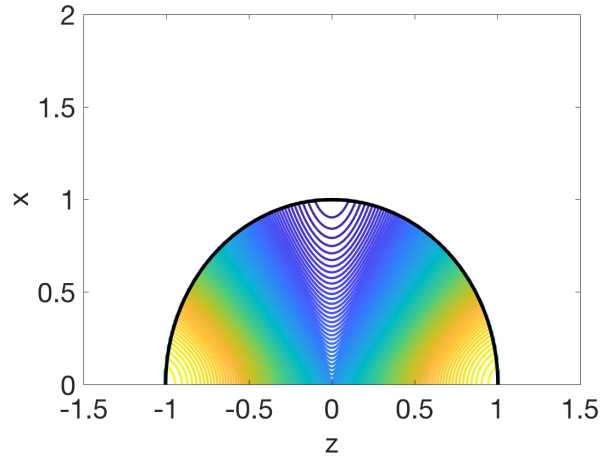
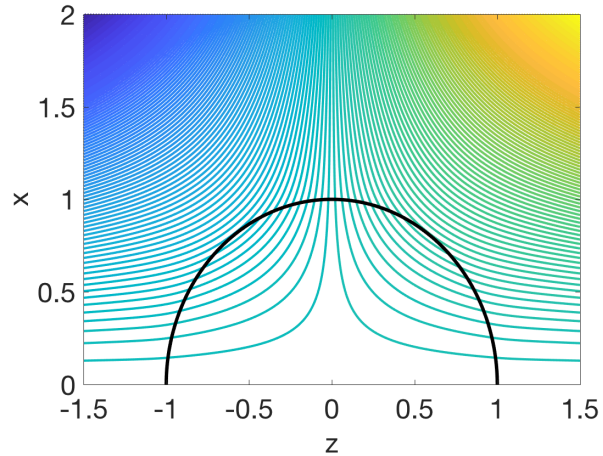
$$\mathbf{v}_{s,e} \cdot \hat{\mathbf{r}} = \left(-\frac{3(5 - 2\Lambda)}{25}d_1r^3 - d_2r - \frac{2\Lambda}{7 + 3\Lambda}d_3r^3 \right) (1 + 3 \cos(2\theta)),$$

$$\mathbf{v}_{s,e} \cdot \hat{\boldsymbol{\theta}} = \left(\frac{3(6 - \Lambda)}{25}d_1r^3 + d_2r + \frac{1}{3}d_3r^3 \right) \sin(2\theta),$$

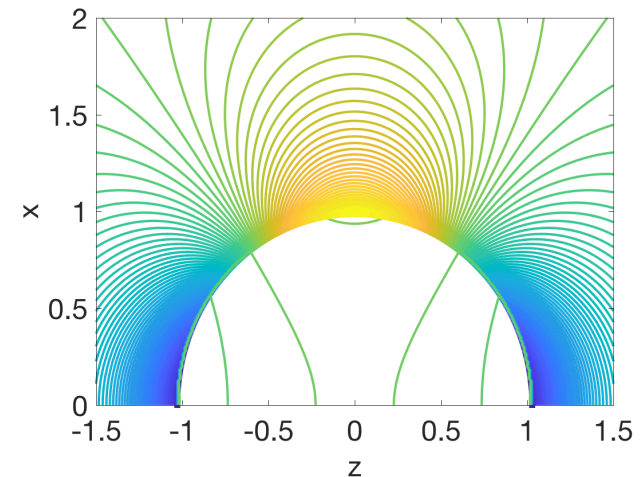
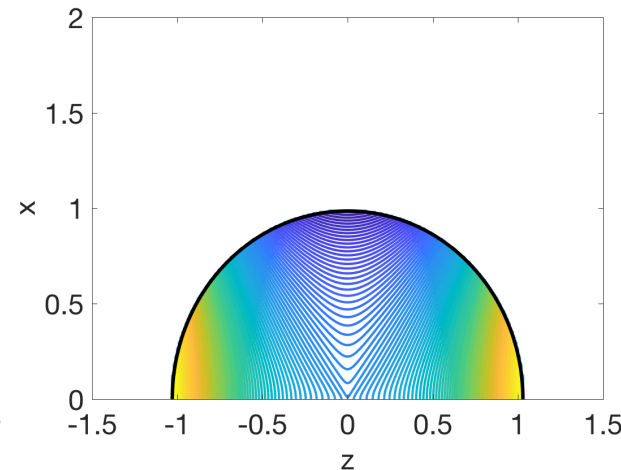
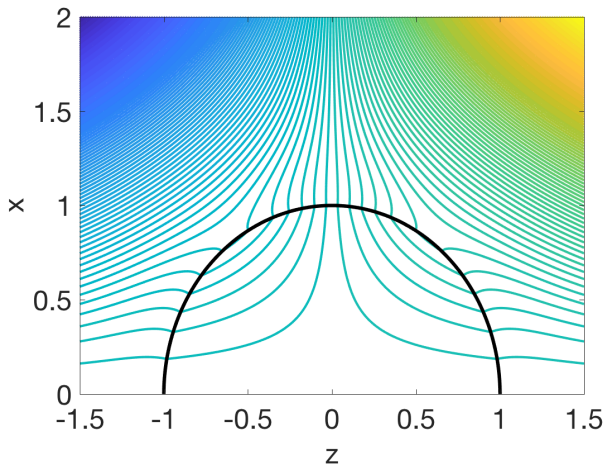
$$\psi_e = E \left(r^3 - \frac{A_1}{2} - \frac{A_2}{2r^2} \right) \cos \theta \sin^2 \theta,$$

$$P = -\frac{\alpha_e}{2r^3}A_1 (1 + 3 \cos(2\theta)).$$

Flow around a soft Darcy drop in a uniaxial extensional flow: equilibrium



- $\Lambda/M=1/3, \phi_0=0.8, \beta=10^3, \eta_1=10, \xi=1$



- $\Lambda/M=1/3, \phi_0=0.8, \beta=0, \eta_1=10, \xi=1$

Small-deformation of a Darcy drop in a planar shear flow

$$p_e = \frac{G}{2} d_1 r^2 \sin^2 \theta \sin(2\phi),$$

$$\mathbf{v}_{e,s} \cdot \hat{r} = \left(\frac{G}{7(1-\Lambda)(1-\phi_0)} d_1 r^3 + d_3 r + \frac{2\Lambda}{7+3\Lambda} d_4 r^3 \right) \sin^2 \theta \sin(2\phi),$$

$$\mathbf{v}_{e,s} \cdot \hat{\theta} = \left(\frac{5G}{21(1-\Lambda)(1-\phi_0)} d_1 r^3 + d_3 r + \frac{1}{3} d_4 r^3 \right) \sin \theta \cos \theta \sin(2\phi),$$

$$\mathbf{v}_{e,s} \cdot \hat{\phi} = \left(-\frac{Gt}{2} r + \left(\frac{5G}{21(1-\Lambda)(1-\phi_0)} d_1 r^3 + d_3 r + \frac{1}{3} d_4 r^3 \right) \cos(2\phi) \right) \sin \theta,$$

$$\mathbf{U}_e \cdot \hat{r} = \frac{G}{20r^4} (6C_3 + 5C_1 r^2 + 10r^5) \sin^2 \theta \sin(2\phi),$$

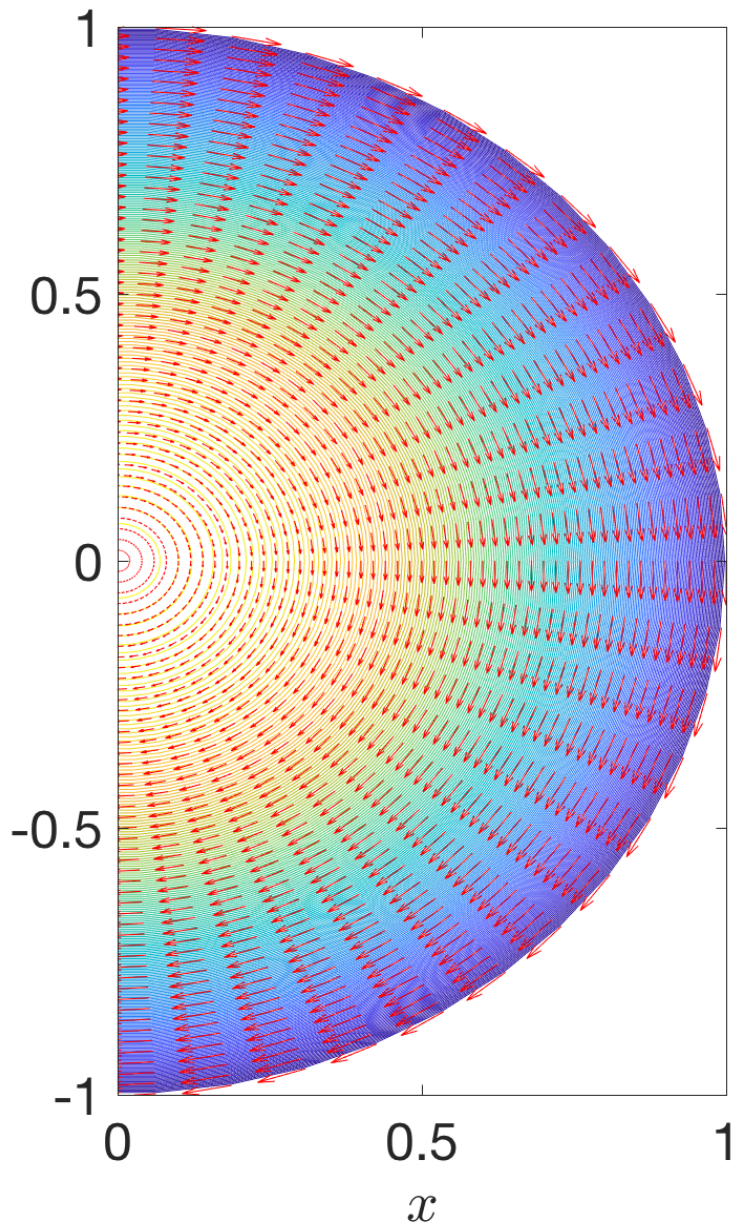
$$\mathbf{U}_e \cdot \hat{\theta} = \frac{G}{20r^4} (-2C_3 + 5r^5) \sin(2\theta) \sin(2\phi),$$

$$\mathbf{U}_e \cdot \hat{\phi} = -\frac{G}{10r^4} (5(2C_4 r^2 + r^5) + (2C_3 - 5r^5) \cos(2\phi)) \sin \theta,$$

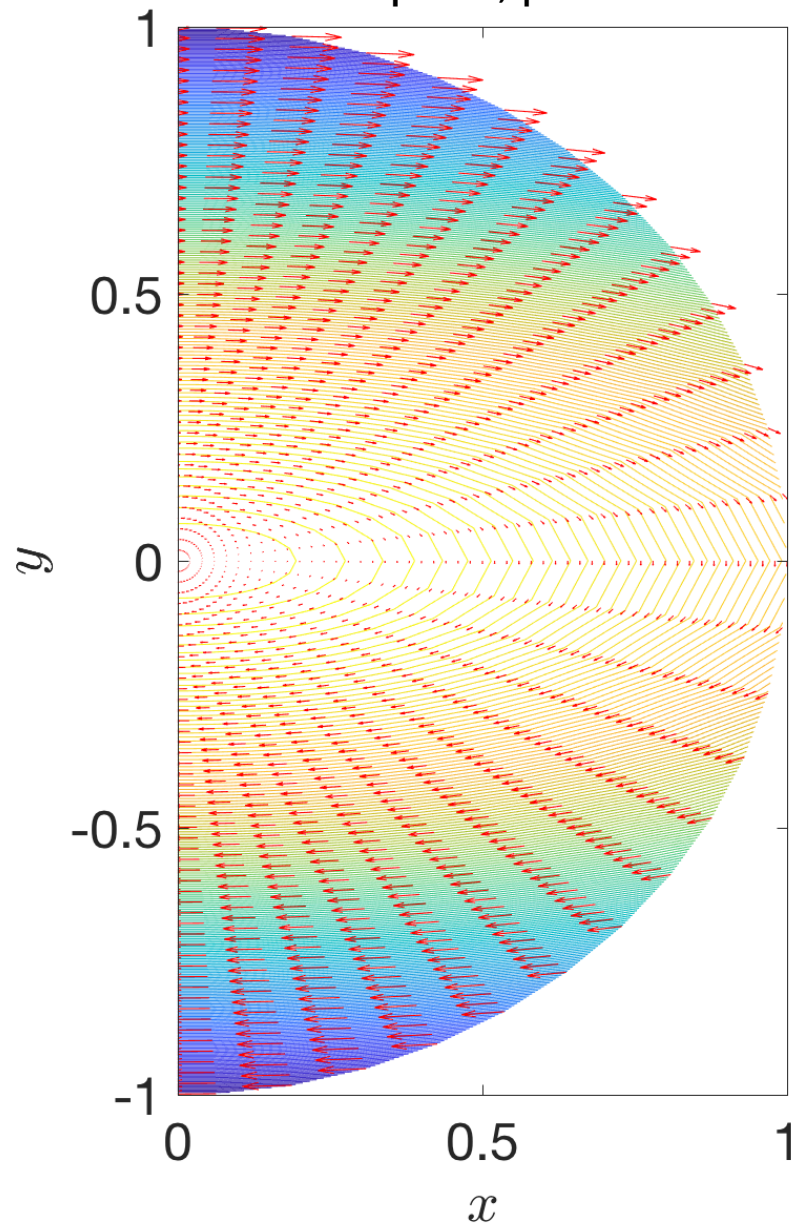
$$P_e = \frac{G\alpha_e}{2r^3} C_1 \sin^2 \theta \sin(2\phi).$$

Small-deformation of a Darcy drop in a planar shear flow

• $\eta=0, \beta=0$



• $\eta=100, \beta=0$



Linear dynamics of a Darcy drop in a uniaxial extensional flow

$$\mathbf{v}_{s,1} \cdot \hat{\mathbf{r}} = \frac{h_0(r)}{3} (1 + 3 \cos(2\theta)) e^{\lambda t},$$

$$\mathbf{v}_{s,2} \cdot \hat{\boldsymbol{\theta}} = h_1(r) \sin(2\theta) e^{\lambda t},$$

$$p_1 = \frac{(1 - \phi_0)}{12r} [(8(1 + \lambda\mu_s)h_0 + 2(1 + \Lambda + \lambda\mu_s)rh'_0) +$$

$$(\dots + 9)) e^{\lambda t},$$

$$h_0 = g_1(r) = r^5 + \frac{2\bar{\lambda}}{99}r^7 + \frac{5\bar{\lambda}^2}{20592}r^9 + \frac{\bar{\lambda}^3}{514800}r^{11} + \dots,$$

$$h_1 = g_2(r) = \frac{28}{\bar{\lambda}}r^3 - \frac{1}{3}r^5 - \frac{\bar{\lambda}}{198}r^7 - \frac{\bar{\lambda}^2}{20592}r^9 - \frac{\bar{\lambda}^3}{3088800}r^{11} + \dots,$$

$$\psi_{e,1} =$$

$$P_1 = -\frac{\alpha_e}{2r^3}a_1 (1 + 3 \cos(2\theta)), \quad \bar{\lambda} \equiv \frac{\lambda\xi}{(1 + \lambda\mu_s)\phi_0}.$$

Linear dynamics of a Darcy drop in a planar shear flow

$$\mathbf{v}_{s,1} \cdot \hat{\mathbf{r}} = f_0(r) \sin^2 \theta \sin(2\phi) e^{\lambda t},$$

$$\mathbf{v}_{s,1} \cdot \hat{\boldsymbol{\theta}} = \frac{f_1(r)}{2} \cos(2\theta) \sin(2\phi) e^{\lambda t},$$

$$\mathbf{v}_{s,1} \cdot \hat{\boldsymbol{\phi}} = f_1(r) \sin \theta \cos(2\phi) e^{\lambda t},$$

$$p_1 = \frac{(1 - \phi_0)}{4r} [(8(1 + \lambda\mu_s) f_0 + 2(1 + \Lambda + \lambda\mu_s) r f_0') - (12(1 + \lambda\mu_s) f_1 - 2(1 - \Lambda + \lambda\mu_s) r f_1' - 2(1 - \Lambda + \lambda\mu_s) r^2 f_1'')] (1 + 3 \cos(2\theta)) e^{\lambda t},$$

$$f_0 = \alpha_1 r + \alpha_3 r^3 + \alpha_5 g_1(r),$$

$$f_1 = \alpha_1 r + \frac{5}{3} \alpha_3 r^3 - \alpha_5 g_2(r),$$

$$\mathbf{A} \begin{pmatrix} \alpha_1 \\ \alpha_3 \\ \alpha_5 \end{pmatrix} = \lambda \mathbf{B}_0 \begin{pmatrix} \alpha_1 \\ \alpha_3 \\ \alpha_5 \end{pmatrix}$$

$$\mathbf{U}_1 \cdot \hat{\mathbf{r}} = \frac{G}{20r^4} (c_3 + 5c_1 r^2) \sin^2 \theta \sin(2\phi) e^{\lambda t},$$

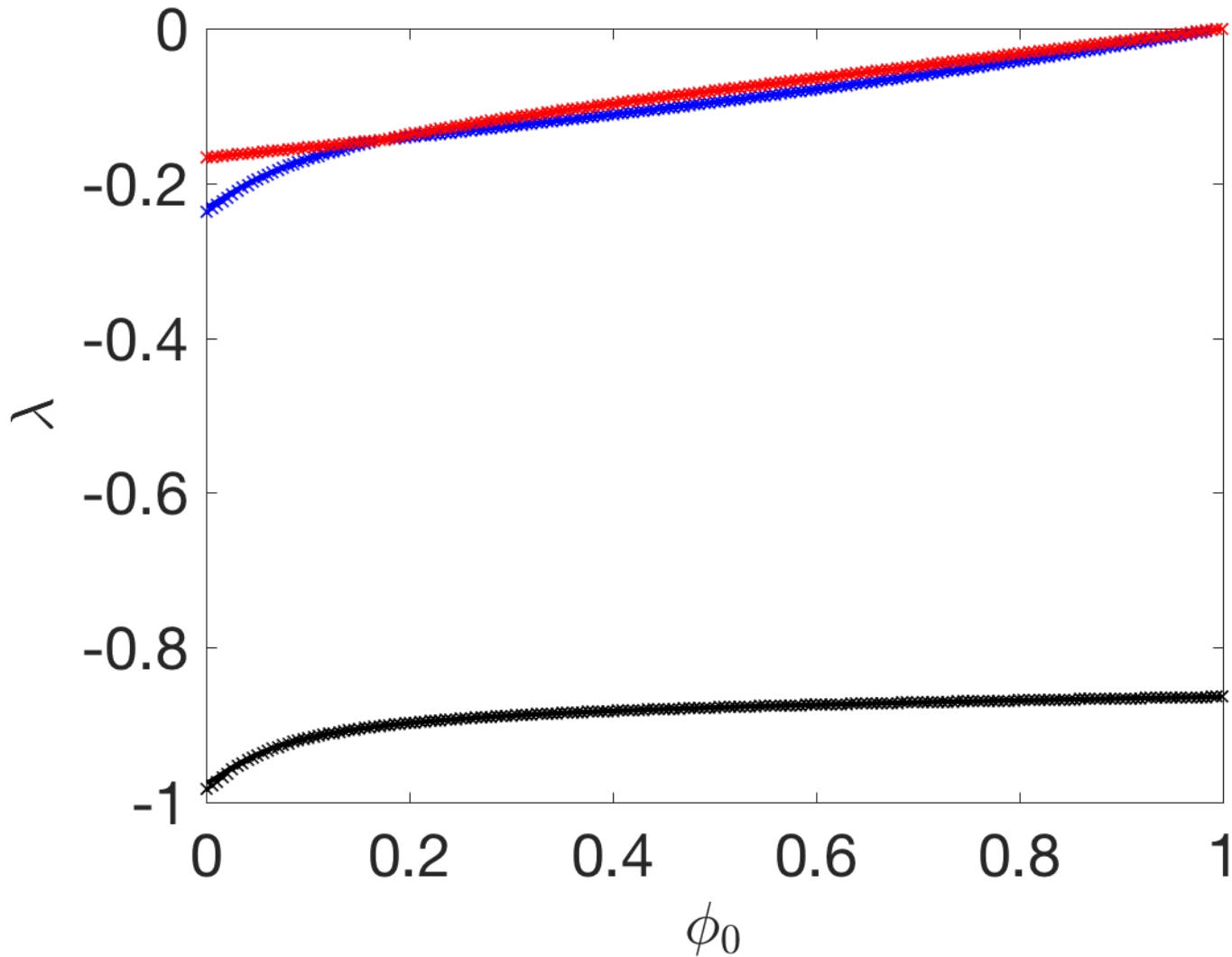
$$\mathbf{U}_1 \cdot \hat{\boldsymbol{\theta}} = -\frac{G}{10r^4} c_3 \sin(2\theta) \sin(2\phi) e^{\lambda t},$$

$$\mathbf{U}_1 \cdot \hat{\boldsymbol{\phi}} = -\frac{G}{10r^4} (10c_4 r^2 + 2c_3 \cos(2\phi)) \sin \theta e^{\lambda t},$$

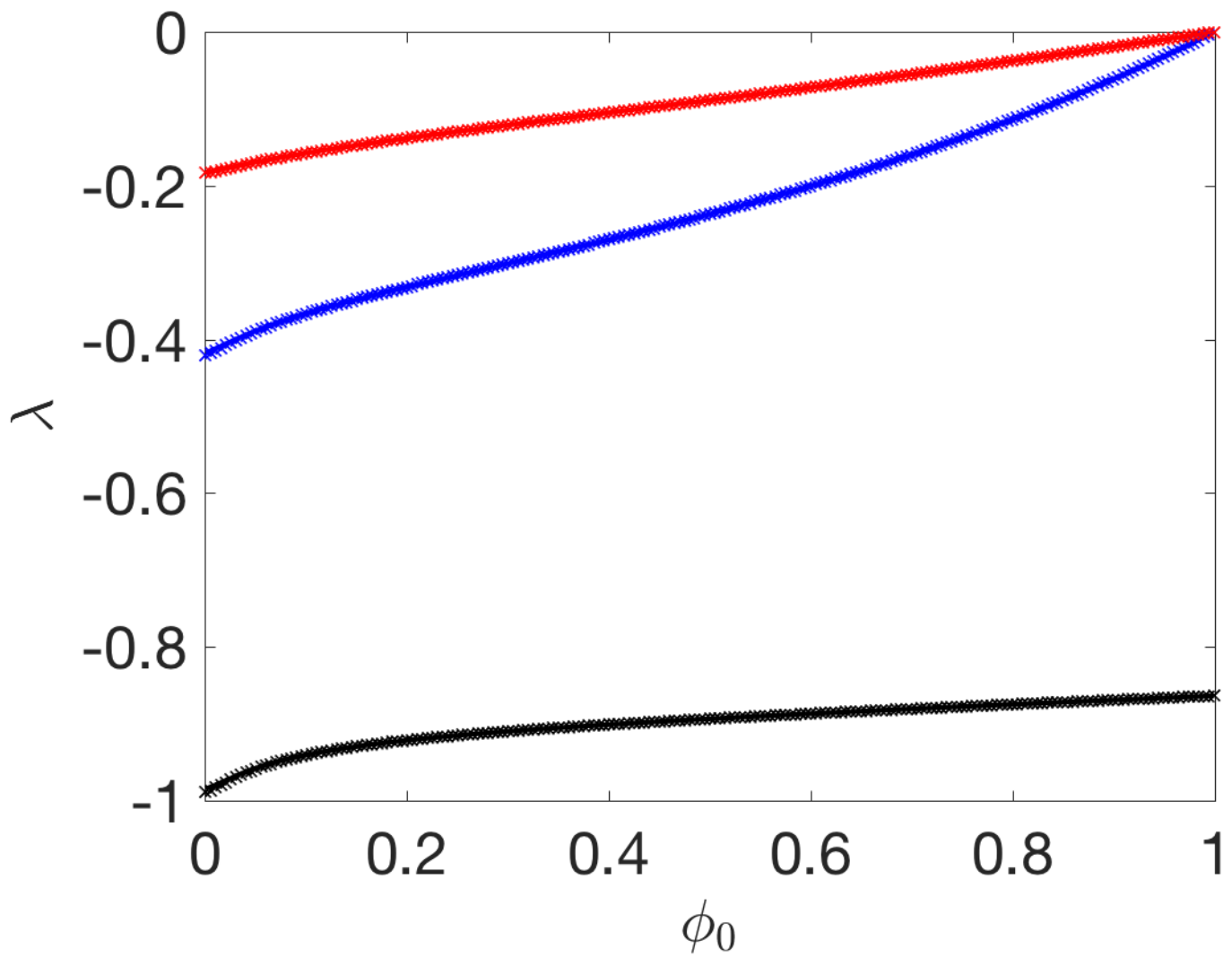
$$\frac{\xi \lambda}{(1 + \mu_s \lambda) \phi_0} \rightarrow \frac{\xi}{\mu_s \phi_0} \text{ as } \mu_s |\lambda| \gg 1$$

$$P_1 = \frac{G \alpha_e}{2r^3} c_1 \sin^2 \theta \sin(2\phi) e^{\lambda t}.$$

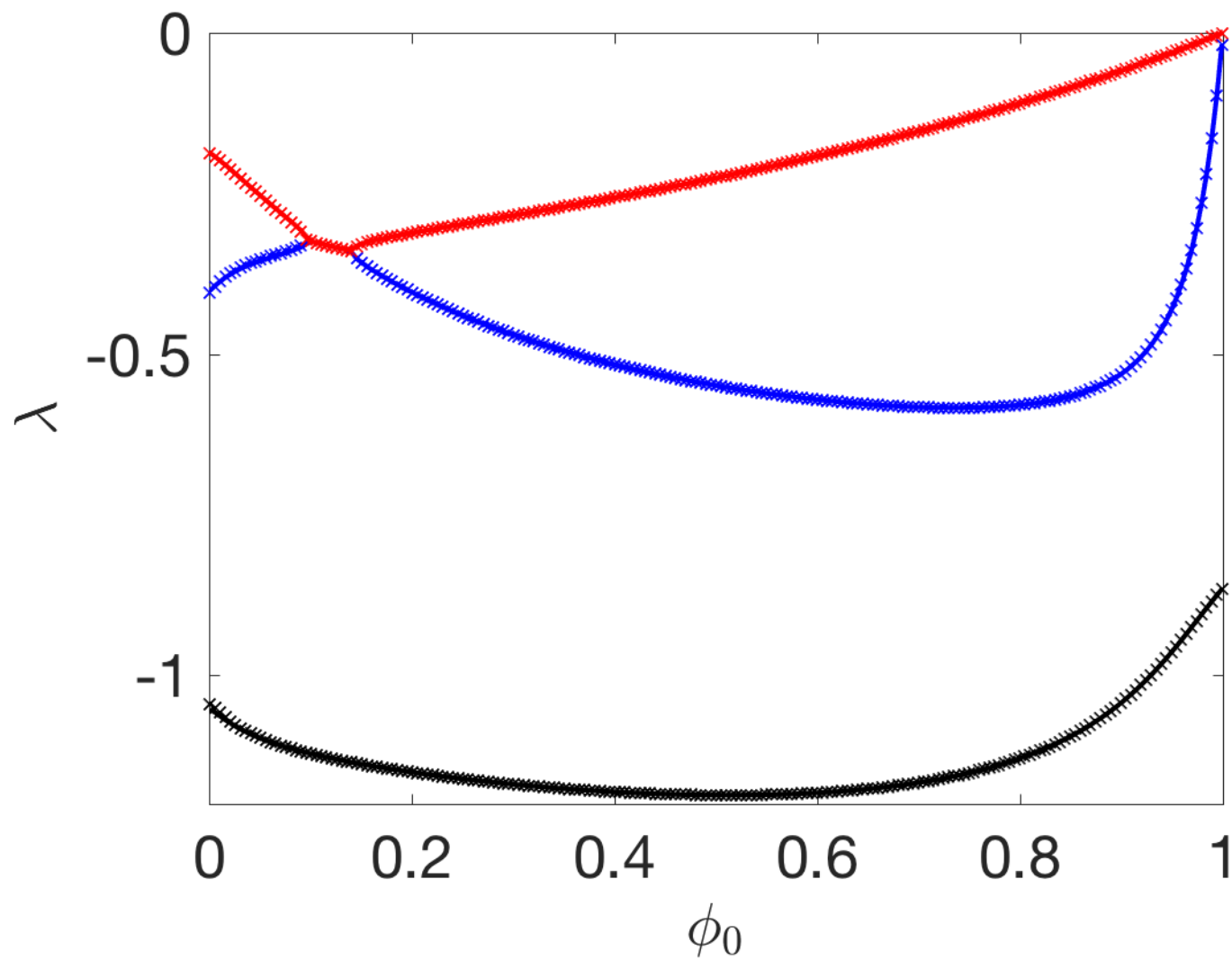
Linear dynamics of small-deformation of a Darcy drop: $\beta=0, \eta_1=0$



Linear dynamics of small-deformation of a Darcy drop: $\beta=1, \eta_1=0$



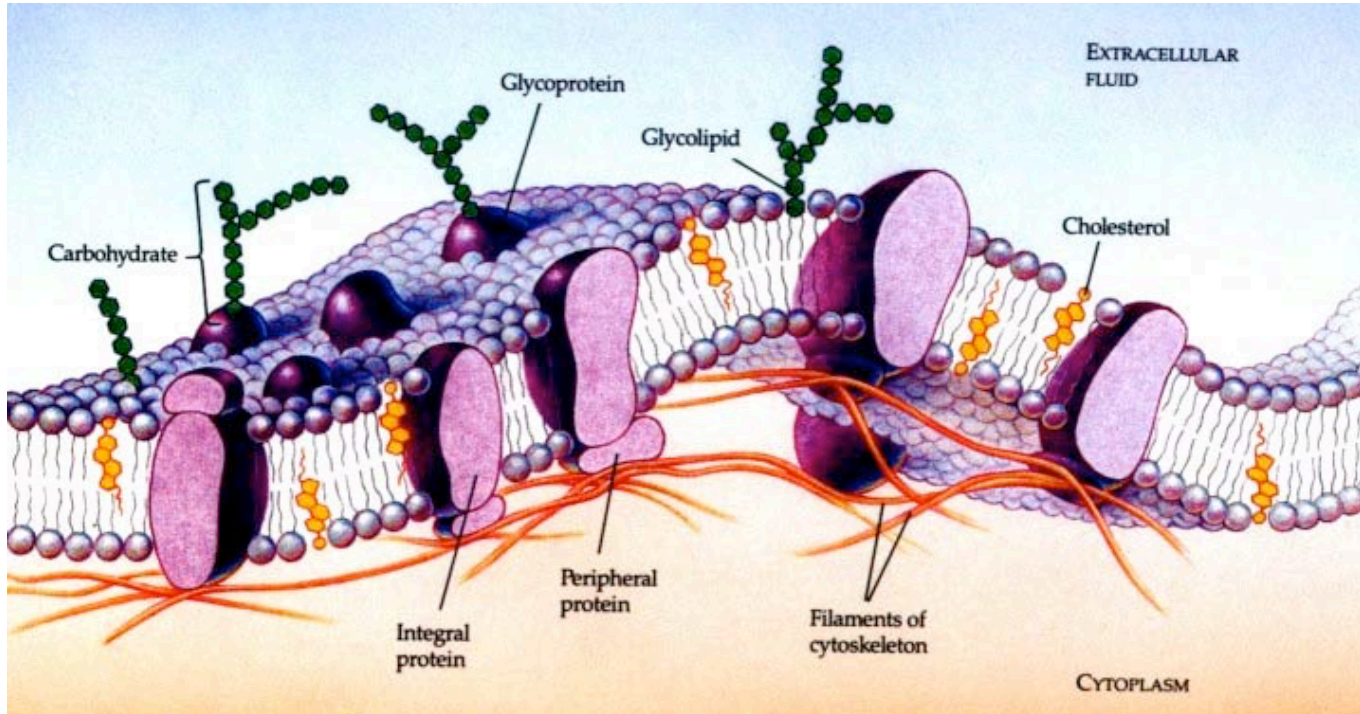
Linear dynamics of small-deformation of a Darcy drop: $\eta_1=20$



Conclusion and ongoing work

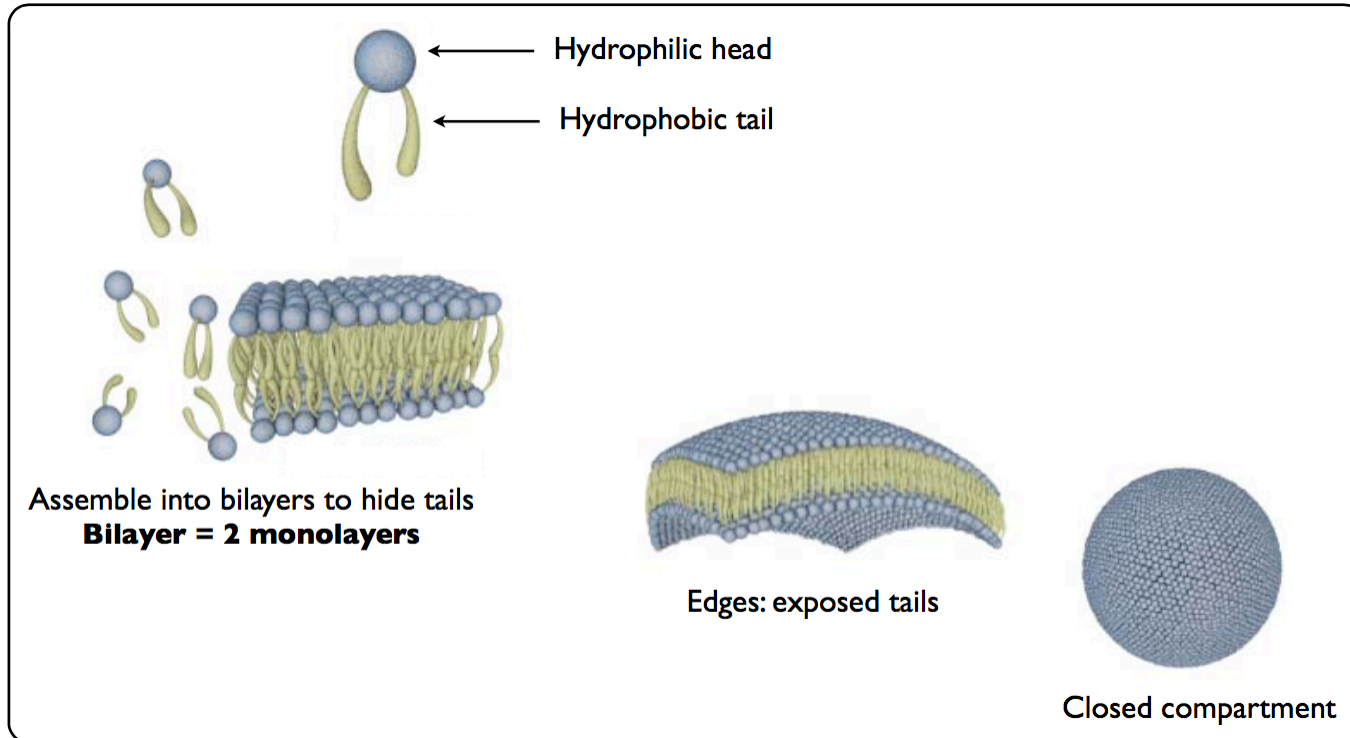
- Both permeability and slip change the flow around the soft drop even in the small-deformation limit.
- Soft poroelastic drop in extensional flow and shear flow. Brinkman drop is also considered (in a separate paper).
- Large deformation of soft poroelastic drop in Stokes flow? (Strychalski *et al*, JCP, 2014, Wrobel *et al.*, JFM, JCP, 2016)
- Swelling and charge transport and electrohydrodynamics of polyelectrolytic solution?

Cell membrane



- A drawing of a cellular cytoplasmic membrane.

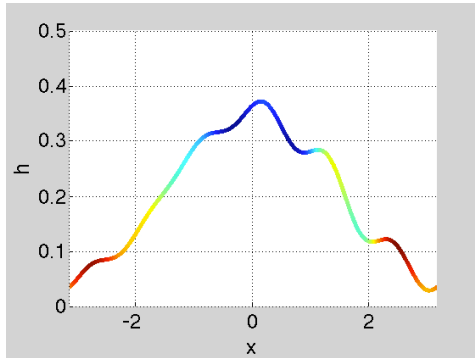
Structures of lipid bilayer membranes



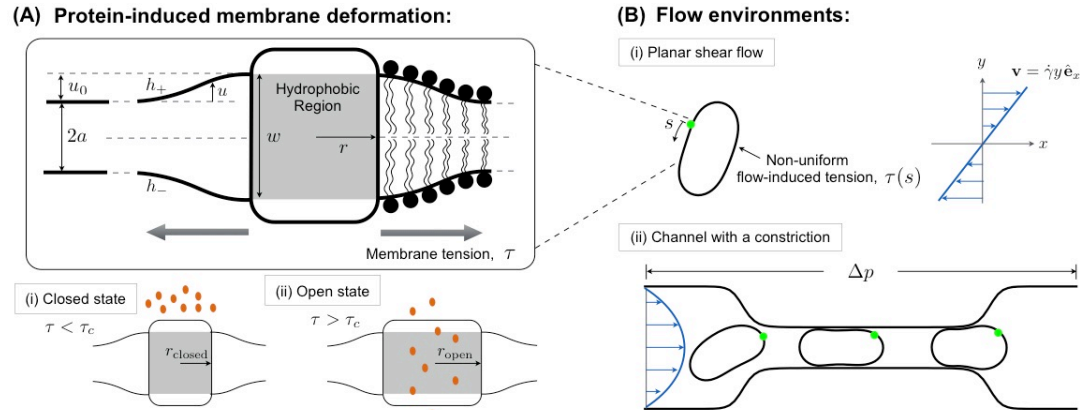
- Bilayer of thickness $2a \sim 5$ nm with a bending modulus κ , area stretching modulus K , membrane conductance σ_m and permittivity ϵ_m (membrane capacitance $c_m = \epsilon_m / 2a$)

Hydrodynamics of lipid bilayer membranes

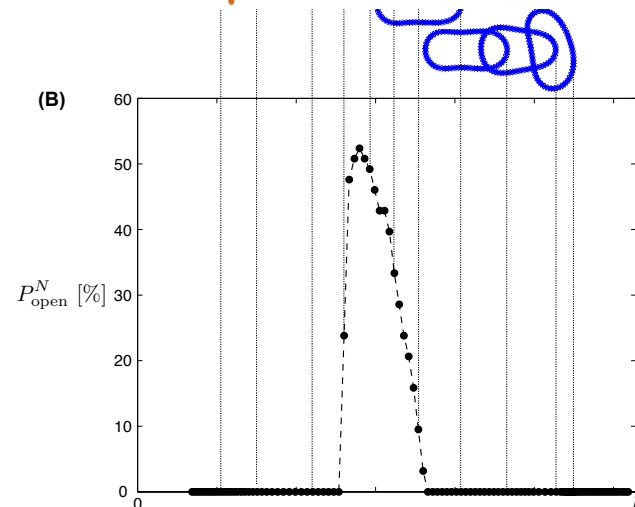
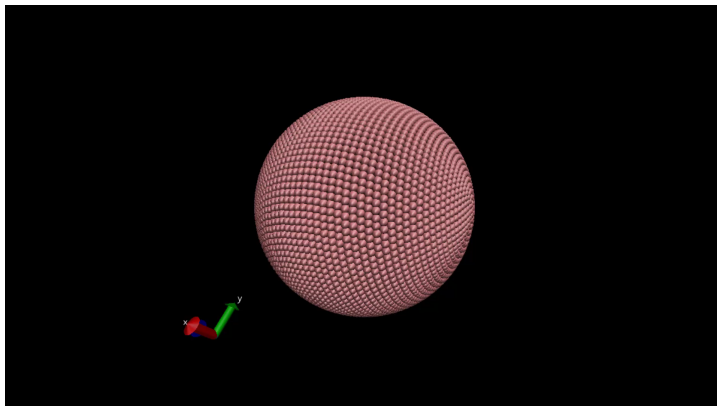
1. Electrohydrodynamics of a planar lipid bilayer membrane (JFM 2014, PoF 2015)



2. Protein-lipid interaction (PNAS 2015, Acta Mechanica Sinica 2016)

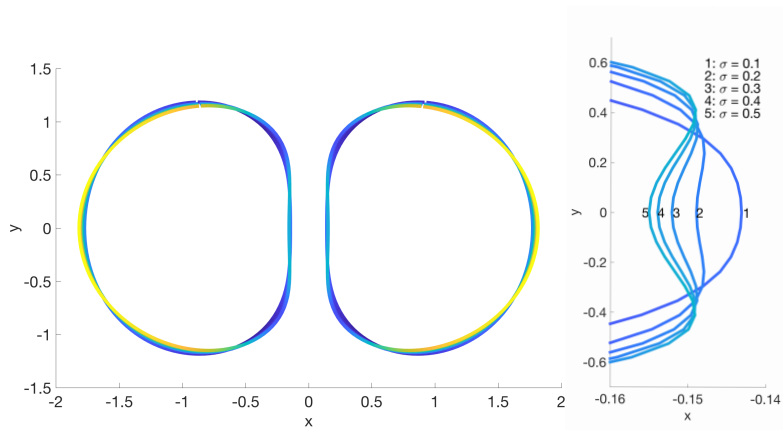


3. Poration of a vesicle (CPC 2017)

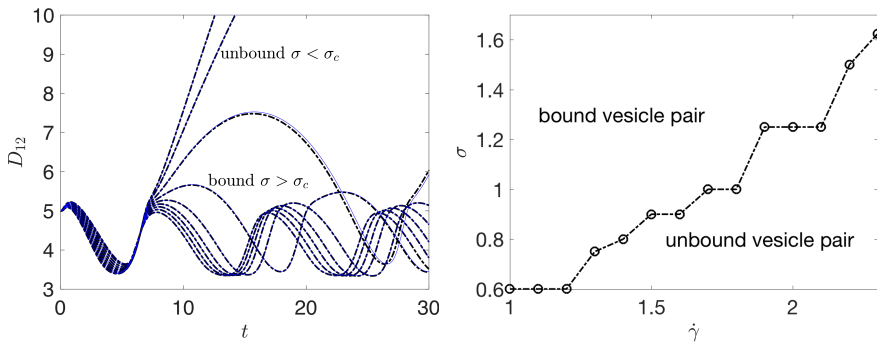


vdW interactions between two vesicles

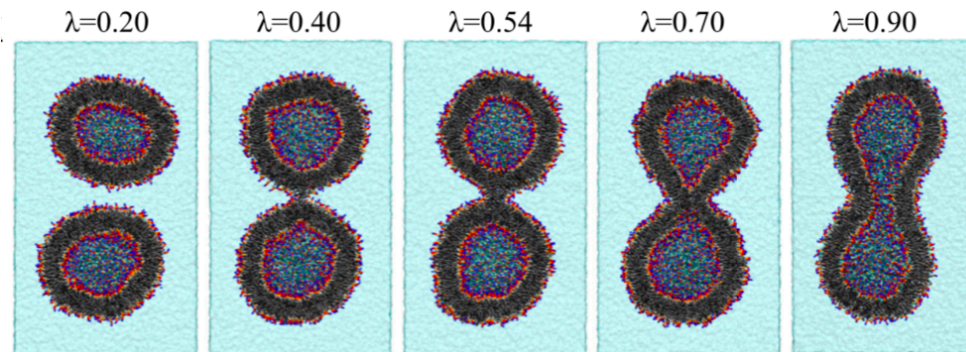
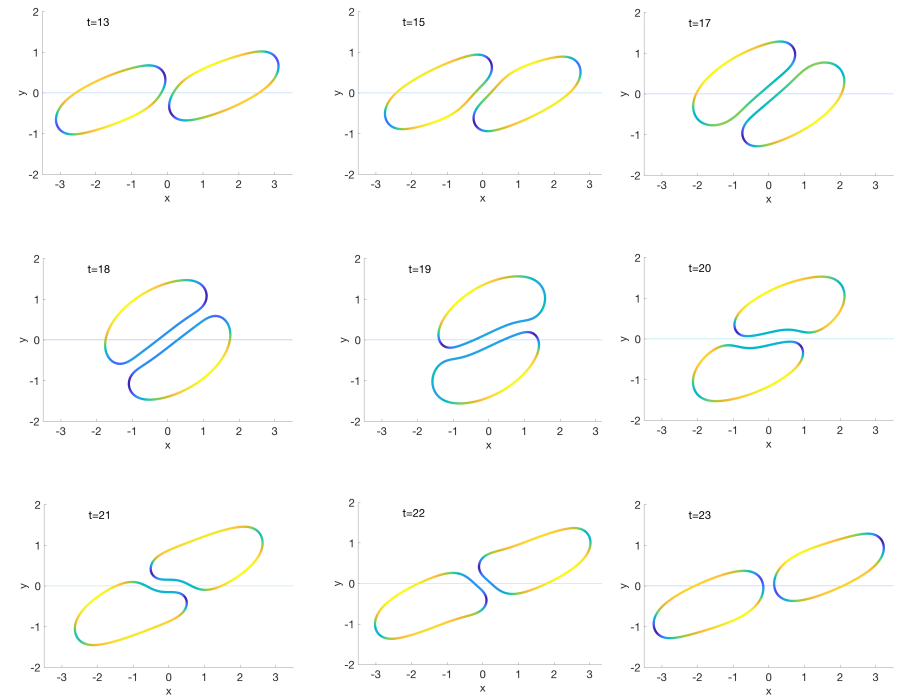
- Two vesicles interacting with each other via a vdW potential



- Two vesicles interacting with each other via a vdW potential under a shear flow

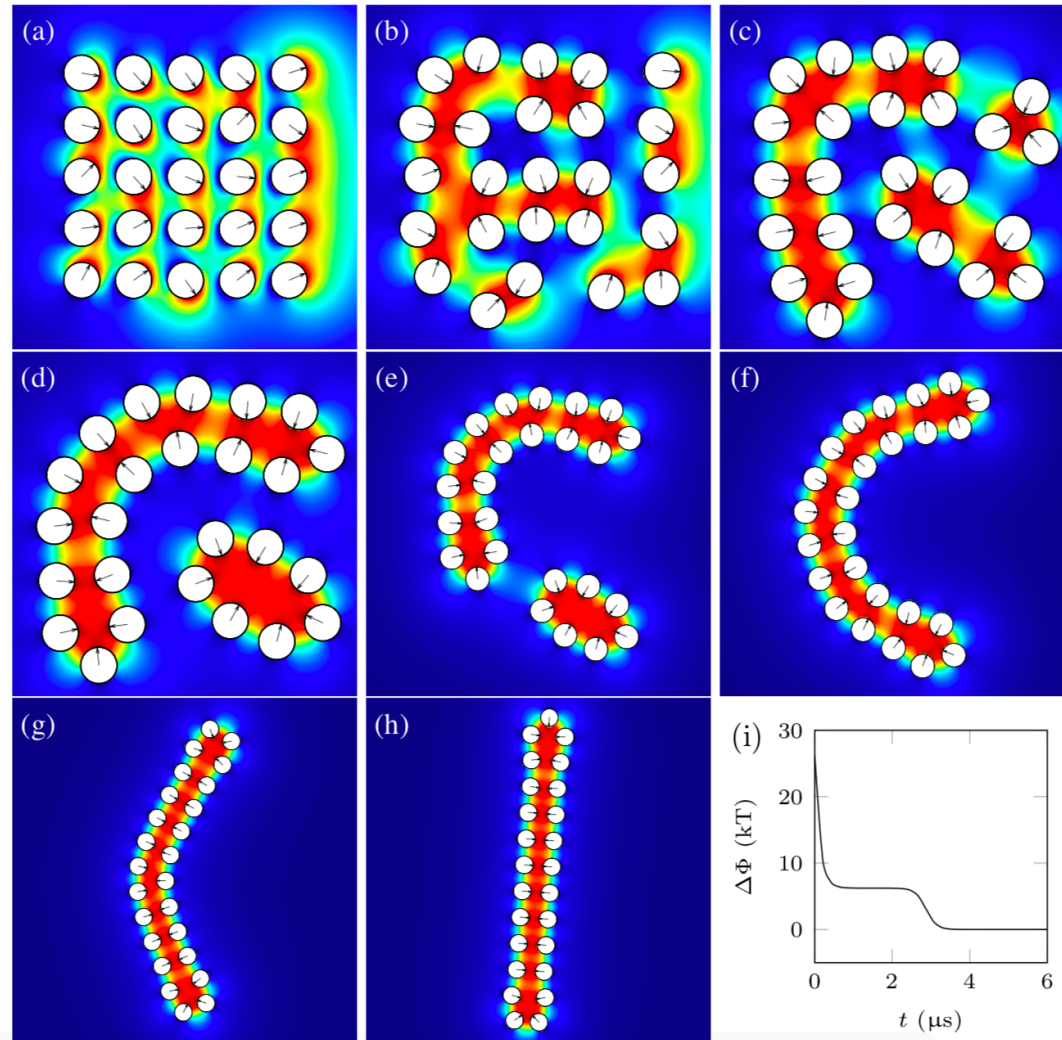


- Hydrodynamics of a vesicle doublet in a shear flow



Hydrophobic interaction as a dominant mechanism

- Splay, saddle splay, tilt and stretching deformations from classic continuum membrane mechanics arise as a consequence of large-scale hydrophobic attraction minimization on membrane-like configurations.
- “Long-range” hydrophobic interaction sufficient to replace Helfrich free energy?
- Fu *et al.*, submitted for publication in SIAM Multiscale Modeling.



A viscous drop in a uniform streaming flow

- Spherical coordinate system
- Interior viscosity increases from top to bottom
- Streamlines around an osmophoretic drop (Anderson, 1981, 1983)

