

Estimation and Control Problems in Systems with Moreau's Sweeping Process

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MS 78 – Dynamics of Moreau Sweeping Process
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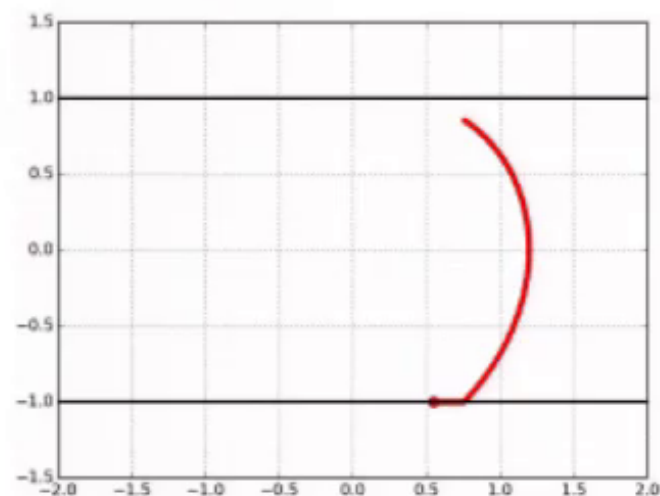
Perturbed Sweeping Processes

First Order Systems

$\mathcal{S} : \mathbb{R}_+ \rightrightarrows \mathbb{R}^n$; $\mathcal{S}(t)$ closed.

$$dx \in f(t, x)dt - \mathcal{N}_{\mathcal{S}(t)}(x)$$

$\mathcal{N}_{\mathcal{S}}(x)$ is the *normal cone* to \mathcal{S} at x .

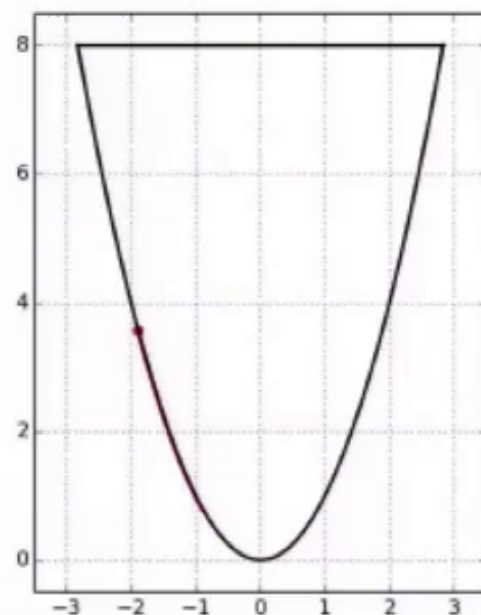


Second Order Systems

$V : \mathbb{R}^n \rightrightarrows \mathbb{R}^n$ is state-dependent.

$$dq = v dt$$

$$dv \in F(t, q, v)dt - \mathcal{N}_{V(q)}(v)$$



Outline

- 1 Generalized First Order Sweeping Process
- 2 Output Regulation with Convex Sets
- 3 State Estimation in Second Order Sweeping Process

Generalizations of First Order Sweeping Process

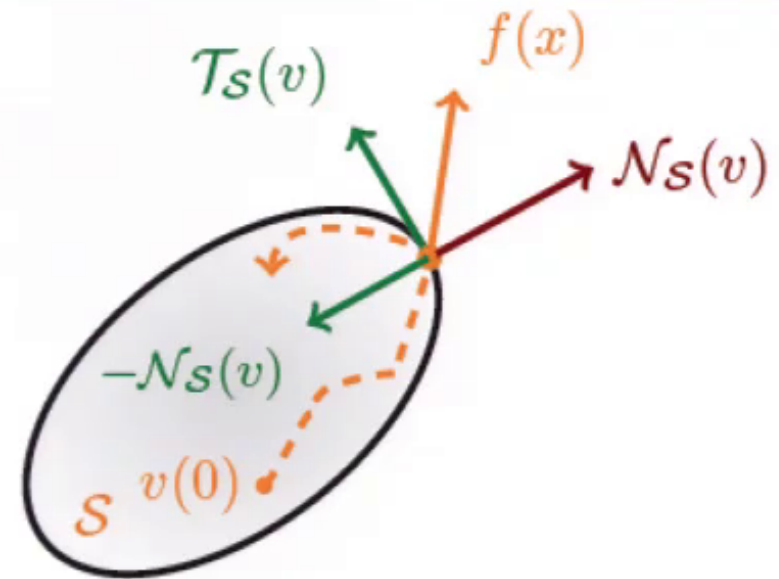
Differential Variational Ineq. (DVI)

Let $\mathcal{S} : \mathbb{R}_+ \rightrightarrows \mathbb{R}^s$ be closed and convex.

$$\dot{x} = f(t, x) + G\eta$$

$$v = Hx + J\eta, \quad v(t) \in \mathcal{S}(t)$$

$$\eta \in -\mathcal{N}_{\mathcal{S}}(v)$$



Generalizations of First Order Sweeping Process

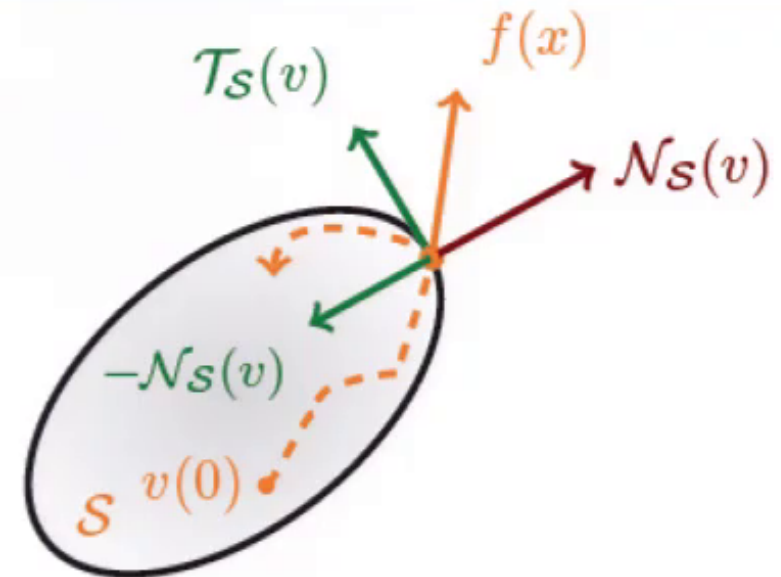
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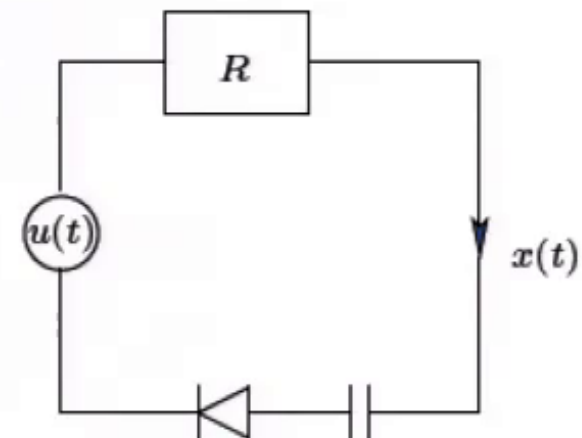
$$v = Hx + J\eta, \quad v(t) \in \mathcal{S}(t)$$

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Linear Complementarity

$$0 \leq \eta \perp v \geq 0$$



- Sweeping Process [Moreau; Monteiro Marques; Colombo; Thibault] and [Participants of MS78, MS91 at SIAM DS'15]
- Evolution Inclusions [Aubin; Celina]
- DVIs & complementarity [Cottle; Pang; Stone; Stewart]

Existence and Uniqueness of Solutions for DVI's [CDC '14]

$$\text{(DVI)} : \dot{x} = f(t, x) + G\eta, \quad \eta \in -\mathcal{N}_{\mathcal{S}}(Hx + J\eta)$$

Theorem (Sufficient Conditions for Well-posedness of DVI)

There exists a unique absolutely continuous (a.c.) solution of **(DVI)**, if

(A1) $J \geq 0$ and $\exists P = P^\top > 0$ s.t. $\ker(J + J^\top) \subseteq \ker(PG - H^\top)$.

(A2) $\text{range } H \cap (\mathcal{S}(t) + \text{range } J) \neq \emptyset, \forall t \geq 0$.

(A3) The mapping $t \mapsto \mathcal{S}(t)$ is a.c., i.e., \exists an a.c. function $\nu(\cdot) : [0, \infty) \rightarrow \mathbb{R}_+$ s.t.

$$|d(v, \mathcal{S}(t_1)) - d(v, \mathcal{S}(t_2))| \leq |\nu(t_1) - \nu(t_2)|, \quad \forall t_1, t_2 \geq 0.$$

(A4) $f(t, x)$ is globally Lipschitz in x and a.c. in t .

- There exists an operator Φ s.t. $\dot{x}(t) \in f(t, x) - G\Phi(t, Hx(t))$.
- Under **(A1)**, **(A2)**, \exists a maximal monotone operator $\Psi(t, \cdot)$, a Lipschitz continuous function $g(t, \cdot)$, and a transformation $z = Rx$ s.t.

$$\dot{z}(t) \in g(t, z) - \Psi(t, z)$$

- Earlier results only consider the case $J = 0$ or J positive definite.

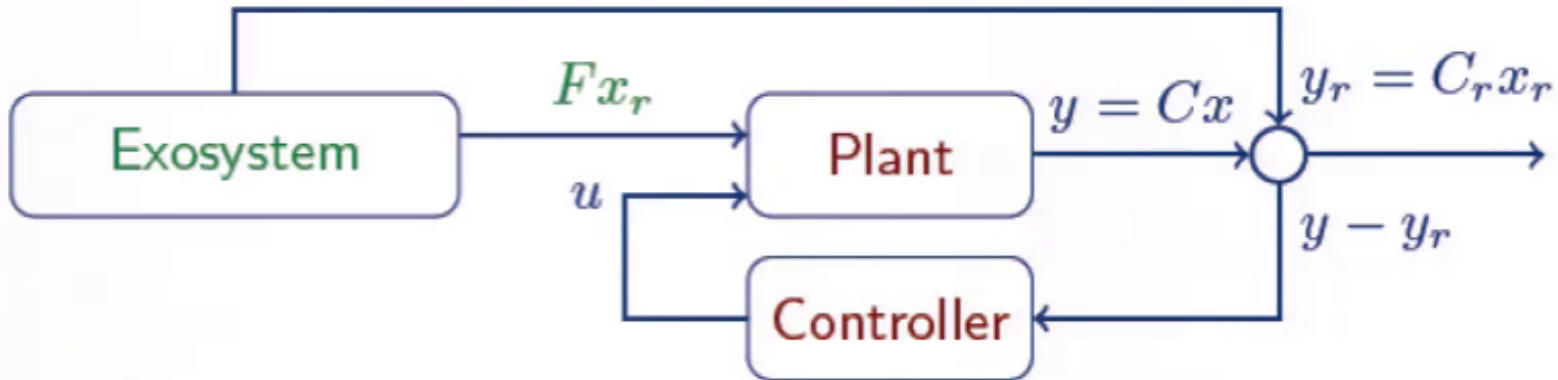
Outline



Control design: Exchange information between systems so that a subset of **System 1** trajectories track a subset of **System 2** trajectories.

- 1 Generalized First Order Sweeping Process
- 2 Output Regulation with Convex Sets
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Regulation Problem



Exosystem (Ref. Generator)

$$\begin{aligned}\dot{x}_r &= A_r x_r + G_r \eta_r \\ \eta_r &\in -\mathcal{N}_{\mathcal{S}}(H_r x_r + J_r \eta_r)\end{aligned}$$

Plant Dynamics

$$\begin{aligned}\dot{x} &= Ax + Bu + Fx_r + G\eta \\ \eta &\in -\mathcal{N}_{\mathcal{S}}(Hx + J\eta)\end{aligned}$$

Motivation: Such exosystems can generate **nonsmooth** trajectories.

Output Regulation (OR) Problem

Design the control input u such that

- The resulting closed loop system is well-posed
- The regulation error $w = Cx - C_r x_r$ converges asymp. to zero
- The overall closed-loop system is asymp. stable

Regulation with Static Feedback [CDC '14]

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Theorem (Regulator Synthesis Conditions)

Under **(A2)**, **(A3)**, if there exist matrices M, K, Π and $P > 0$ s.t.

- **Passivity of $(A + BK, G, H, J)$:**

$$\begin{bmatrix} (A + BK)^\top P + P(A + BK) + \gamma P & PG - H^\top \\ G^\top P - H & -(J + J^\top) \end{bmatrix} \leq 0$$

- **Internal model (IM):** $\Pi A_r = A\Pi + BM + F \quad \wedge \quad C\Pi - C_r = 0$
- **Constraint matching (CM):** $\Pi G_r = G \quad \wedge \quad H\Pi = H_r \quad \wedge \quad J_r = J$

hold, then **(OR)** is solvable with $u = Kx + (M - K\Pi)x_r$

Tools and Analysis:

- Well-posedness \Leftarrow **(A1)** \Leftarrow Passivity
- Regulation error converges \Leftarrow Internal model principle
- Closed-loop Stability \Leftarrow Constraint matching and passivity

Regulation with Error Feedback [CDC '14]

Premise: Only $w := y - y_r$ is measurable, and full state (x, x_r) is not available.

Dynamic Compensator

For some matrices $\bar{A}, \bar{B}, \bar{C}, \bar{G}, \bar{H}, \bar{J}$, and the set $\bar{\mathcal{S}}$, we let

$$\begin{aligned}\dot{\xi} &= (\bar{A} - L\bar{C})\xi + Lw + \bar{B}u + \bar{G}\bar{\eta}; & \bar{\eta} &\in -\mathcal{N}_{\mathcal{S}}(\bar{H}\xi + \bar{J}\bar{\eta}) \\ u &= K\xi_x + (M - K\Pi)\xi_r\end{aligned}\tag{DC}$$

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Theorem (Regulation with Dynamic Compensator)

- If $(A + BK, G, H, J)$ and $(\bar{A} - L\bar{C}, \bar{G}, \bar{H}, \bar{J})$ are **passive**,
- and the matrices M, Π satisfy **(IM)**, **(CM)** hold

then **(DC)** solves **(OR)**.

- Dynamic compensator is based on certainty equivalence principle, and $\xi := (\xi_x, \xi_r)$ estimates (x, x_r) , which are used by control u .
- Well-posedness and stability follows from similar tools.

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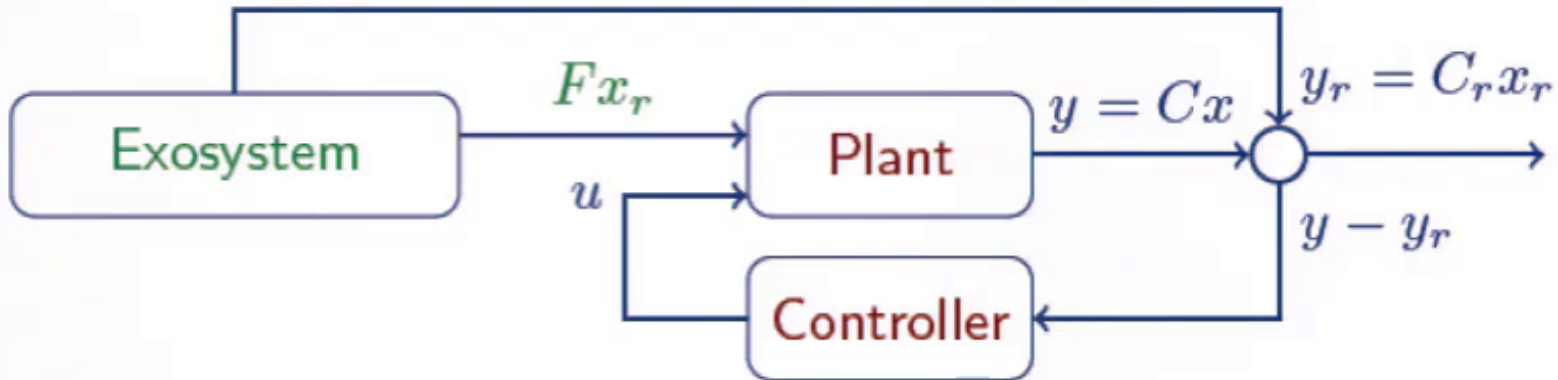
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A Case Study: Regulation with Constraints

Control design for regulation with polyhedral constraints

Plant: $\dot{x} = Ax + Bu$

Constraint set: $\mathcal{S}(t) := \{z \mid z + g(t) \geq 0\}$

Objective: Find u such that $Cx - C_r x_r \rightarrow 0$ and $Hx(t) \in \mathcal{S}(t)$.

Decompose $u = u_{IM} + u_\eta$

Choose $u_{IM} = Kx + (M - K\Pi)x_r$ for regulation using IM principle.

Choose u_η for constraints using **complementarity relations**

$$\begin{aligned}
 & u_\eta(t) \in -\mathcal{N}_{\mathcal{S}(t)}(Hx(t)) \\
 \Leftrightarrow & 0 \leq u_\eta(t) \perp y(t) = Hx(t) + g(t) \geq 0 \\
 \Leftrightarrow & \begin{cases} u_\eta(t) = 0 & \text{if } Hx(t) \in \text{int } \mathcal{S}(t) \\ 0 \leq u_\eta(t) \perp \dot{y}(t) \geq 0 & \text{if } Hx(t) \in \text{bd } \mathcal{S}(t) \end{cases}
 \end{aligned}$$

Limitation: **Relative degree 1** between input and constrained states

Example: Track Clipped Sinusoid with Norm Constraints

Plant: $\dot{x}_1 = -0.1x_1 + x_2, \quad \dot{x}_2 = u.$

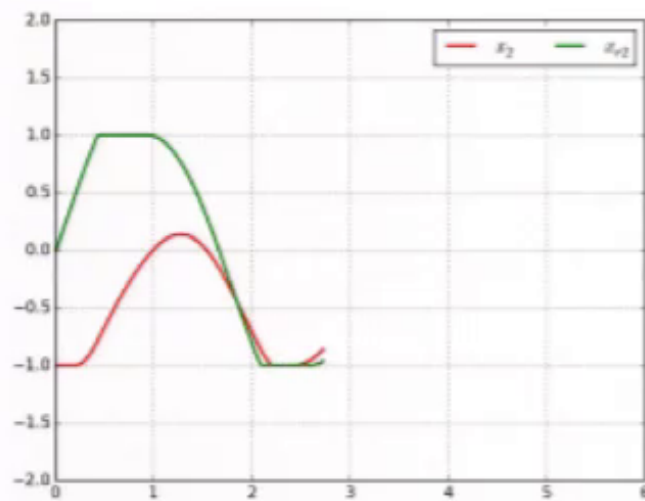
Objective: $x_2(t) \rightarrow x_{r2}(t)$ and $x_2(t) \in \mathcal{S}(t) := \{z : |z| \leq 1\}$

Exosystem (LCS): $\begin{pmatrix} \dot{x}_{r1} \\ \dot{x}_{r2} \end{pmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 1 \end{bmatrix} x_r + \begin{bmatrix} 0 & 0 \\ -1 & 1 \end{bmatrix} \eta_r;$

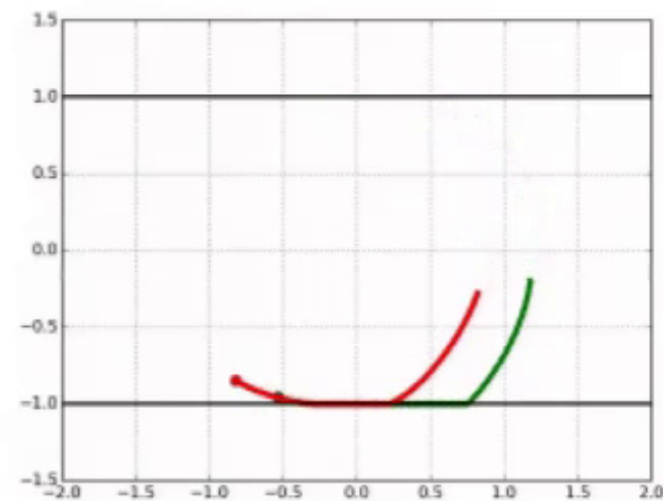
$$0 \leq \eta_r \perp \begin{pmatrix} -x_{r2} \\ x_{r2} \end{pmatrix} + \begin{pmatrix} 1 \\ 1 \end{pmatrix} \geq 0$$

Control: $u = u_{IM} + u_{\eta 1} + u_{\eta 2}$, where $u_{IM} = K_1 x + K_2 x_r$, and

$$0 \leq \begin{pmatrix} -u_{\eta 1} \\ u_{\eta 2} \end{pmatrix} \perp \begin{pmatrix} -x_2 \\ x_2 \end{pmatrix} + \begin{pmatrix} 1 \\ 1 \end{pmatrix} \geq 0$$



(a) Time evolution



(b) Phase portrait

Second Order Processes: Mechanical Systems with Impacts

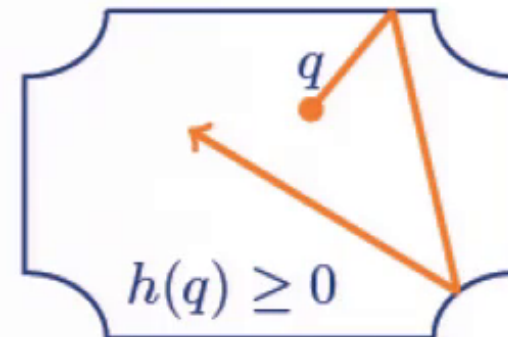
- **Unconstrained motion:**

$$M(q)\dot{v} + F(t, q, v) = 0$$

- **Constraints:**

$$h_i(q) \geq 0$$

- **An impact (jump) rule.**



Second Order Processes: Mechanical Systems with Impacts

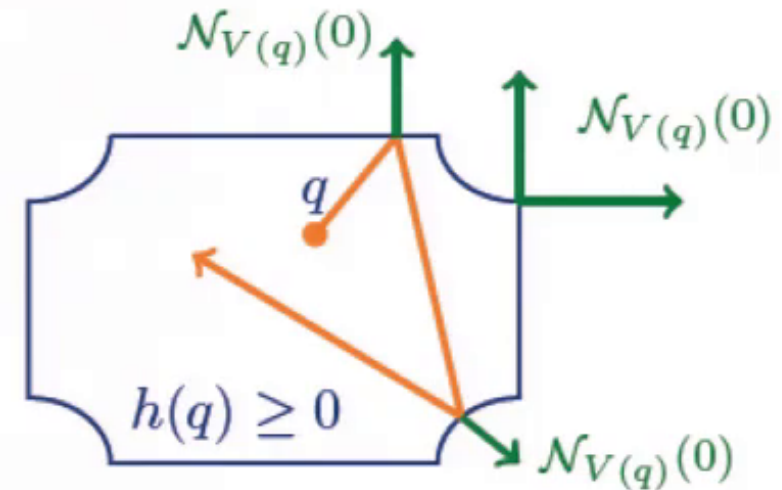
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Sweeping Process Formulation

Velocity set at $h_i(q) = 0$:

$$V(q) := \{w \in \mathbb{R}^n \mid \langle w, \nabla_q h_i(q) \rangle \geq 0\}$$

System description:

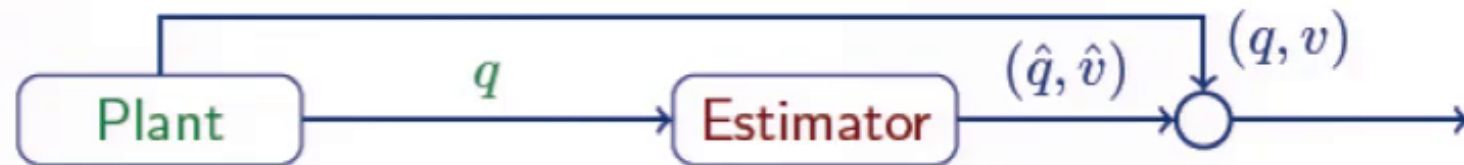
$$\dot{q} = v$$

$$M(q)dv + F(t, q, v)dt \in -\mathcal{N}_{V(q)}(v_e),$$

$$v_e = \frac{v^+ + ev^-}{1 + e}$$

- v is *rcbv* with countably many discontinuities.
- Existence (and uniqueness) holds under mild assumptions (analyticity).
- Solution, in general, is not continuous with respect to initial conditions.

Estimator Dynamics [CDC '13; Submitted to TAC '14]



Our proposed estimator is a **first order** sweeping process:

$$\begin{aligned} \dot{z}_1 &= F_1(t, q, z) \\ M(q)dz_2 + F_2(t, q, z)dt &\in -\mathcal{N}_{V(q)}(\hat{v}_e) \quad (\text{obs}) \\ \hat{q} &= g_1(z_1, q), \quad \hat{v} = z_2 + g_2(z_1, q). \end{aligned}$$

- In **(obs)**, the set-valued map $V(\cdot)$ is parameterized by the external state q of the plant.
- Position estimated by the estimator \hat{q} **does not** satisfy the constraints: $h_i(\hat{q}) \geq 0$.
- $V(\cdot)$ is lower semi-continuous and does not satisfy the “usual” nonempty interior condition.
- The **(obs)** admits a unique solution for an observed trajectory $q(\cdot)$, even if the plant does not have unique solutions.

Results on State Estimation

Let $x := (q, v)$ and $\hat{x} := (\hat{q}, \hat{v})$.

Theorem (Design of Estimator)

Under certain regularity assumption on system data, we can calculate the functions F_1, F_2 and g_1, g_2 such that

- **Well-posedness:** (obs) admits a unique solution
- **Exponential convergence:** $|\hat{x}(t) - x(t)| \leq ce^{-\beta t} |x(0) - \hat{x}(0)|$

Error Analysis:

$$\dot{\tilde{q}} = v - \hat{F}_1(t, x, \hat{x})$$

$$M(q)d\tilde{v} + F(t, x) - \hat{F}_2(t, x, \hat{x}) \in -(\eta - \hat{\eta})$$

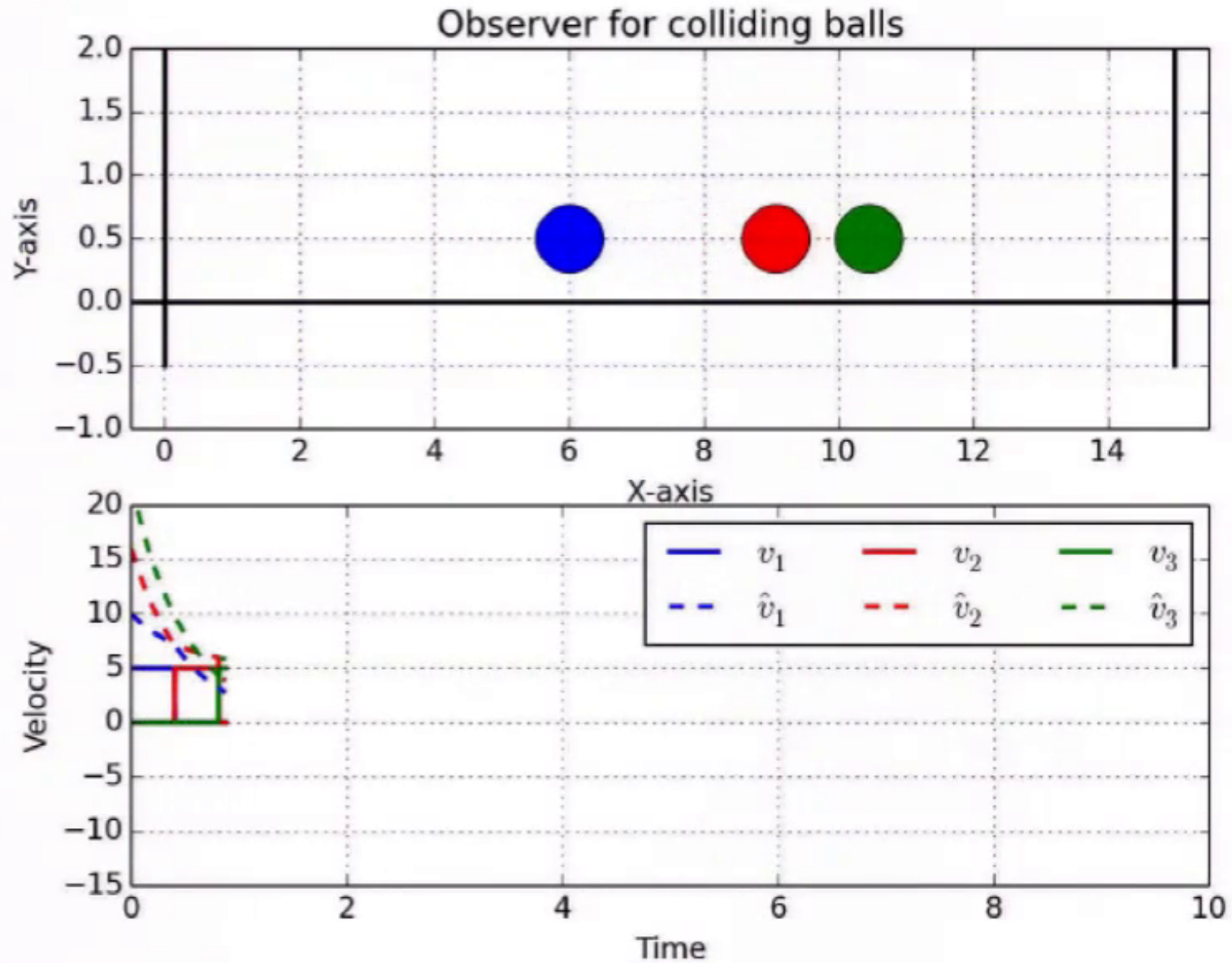
$$\eta \in \mathcal{N}_{V(q)}(v_e) \quad \text{and} \quad \hat{\eta} \in \mathcal{N}_{V(q)}(\hat{v}_e)$$

Induce dissipation in error dynamics (during flows) w.r.t. quadratic Lyapunov function

$$W(q) := \tilde{q}^\top R \tilde{q} + \tilde{v}^\top M(q) \tilde{v}.$$

- Well-posedness result is more involved.

Example: 3-Ball Chain with Walls



Example: A Nonconvex Biliard

Observer for Ball Bouncing in a Hyperbolic Billiard

