# A Quasi-Static Projection Method for 3-Dimensional Hypoelastoplasticity 

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## Bulk Metallic Glasses

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- Solid metal with atoms "frozen" into liquid-like disorder.


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- Solid metal with atoms "frozen" into liquid-like disorder.
- Amorphous structure gives unique properties.


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Crystalline Structure

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Crystalline Structure

## Bulk Metallic Glasses

- Solid metal with atoms "frozen" into liquid-like disorder.
- Amorphous structure gives unique properties.
- Catastrophic failure: shear banding.



Crystalline Structure

## Shear Bands

## Shear Bands

- Localization of stress due to localization of strain.


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- Localization of stress due to localization of strain.
- Strain-softening instability provides positive feedback.


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## Shear Bands

- Localization of stress due to localization of strain.
- Strain-softening instability provides positive feedback.
- Effective temperature $\chi$ quantifies localized "softness".



## Continuum Theory

## Linear Elasticity

## Continuum Theory

Linear Elasticity

$$
\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}: \mathrm{D}^{\mathrm{Del}}
$$

## Continuum Theory

## Linear Elasticity

$$
\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}}_{\text {Jaumann derivative }}=\mathrm{C}: \mathrm{D}^{\mathrm{el}}
$$

Shear Transformation Zone Theory

## Continuum Theory

## Linear Elasticity

Shear Transformation Zone Theory

$$
\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}}_{\text {Jaumann derivative }}=\widetilde{\mathrm{C}}: \mathrm{D}^{\mathrm{el}}
$$

## Continuum Theory

## Linear Elasticity

Shear Transformation Zone Theory

[^0]
## Continuum Theory

## Linear Elasticity

$$
\begin{gathered}
\underbrace{\underset{\mathrm{C}}{\mathrm{Cel}}}_{\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}}_{\text {Jaumn derivative }}=\stackrel{\text { Elastic Part }}{\text { Stiffness }}} \\
\mathrm{D}=\frac{1}{2}\left(\nabla \mathrm{u}+(\nabla \mathrm{u})^{T}\right)
\end{gathered}
$$

## Continuum Theory

## Linear Elasticity

## Shear Transformation Zone Theory

$$
\begin{gathered}
\qquad \underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}}_{\text {Jaumann derivative }}=\stackrel{\sim}{\mathrm{C}}: \underbrace{\text { Stiffness }}_{\text {Elastic Part }} \\
\text { Rate of deformation } \\
\mathrm{D}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }}
\end{gathered}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{gathered}
\begin{aligned}
& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\stackrel{\text { Stiffness }}{\mathrm{C}}: \underbrace{\mathrm{D}^{\mathrm{el}}}_{\text {Elastic Part }} \\
& \text { Jaumann derivative }
\end{aligned} \\
\begin{aligned}
& \mathrm{D}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& \text { Rate of deformation }
\end{aligned} \\
\\
=\mathrm{D}^{e l}+\mathrm{D}^{p l}
\end{gathered}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
& \begin{aligned}
& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\widetilde{\mathrm{C}} \underbrace{\text { Stifness }}_{\text {Elastic Part }} \\
& \text { Jaumann derivative }
\end{aligned} \\
& \begin{aligned}
\mathrm{D}^{\mathrm{Del}}
\end{aligned}=\underbrace{\frac{1}{2}\left(\nabla \mathrm{u}+(\nabla \mathrm{u})^{T}\right)}_{\text {Definition }} \\
&=\underbrace{\mathrm{D}^{e l}+\mathrm{D}^{p l}}_{\text {Refe of deformation }} \\
& \text { Hypoelastoplastic assumption }
\end{aligned}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
\begin{array}{l}
\frac{\mathcal{D} \sigma}{\mathcal{D} t}
\end{array}=\widetilde{\widetilde{C}}: \underbrace{\text { Stiffness }}_{\text {Elastic Part }} \\
\text { Jaumann derivative }
\end{aligned} \underbrace{\mathrm{D}}_{\text {Rate of deformation }}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} .
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
& \underbrace{\mathcal{D} \sigma} \stackrel{\text { Stiffness }}{\mathcal{D} t}=\underbrace{\underset{\mathrm{C}}{\mathrm{D}}}_{\text {Elastic Part }} \\
& \text { Jaumann derivative } \\
& \begin{aligned}
\text { Rate of deformation } & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& =\underbrace{\mathbf{D}^{e l}+\mathrm{D}^{p l}}_{\text {Hypoelastoplastic assumption }}
\end{aligned} \\
& \underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a}=\nabla \cdot \sigma
\end{aligned}
$$

## Shear Transformation Zone Theory

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
& \underbrace{\mathcal{D} \sigma} \stackrel{\text { Stiffness }}{\mathcal{D} t}=\underbrace{\hat{\mathrm{C}}: \underbrace{\mathrm{Del}}}_{\text {Elastic Part }} \\
& \text { Jaumann derivative } \\
& \begin{aligned}
\text { Rate of deformation } & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
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\underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a} & =\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
\end{aligned}
$$

Shear Transformation Zone Theory

## Continuum Theory

## Linear Elasticity

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\begin{aligned}
& \begin{aligned}
& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\widetilde{\mathrm{C}}: \underbrace{\text { Stiffness }}_{\text {Elastic Part }} \\
& \text { Jaumann derivative }
\end{aligned} \\
& \text { Rate of deformation } \\
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& \underbrace{\frac{d \mathbf{u}}{d t}}_{m \times a}=\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
$$

Shear Transformation Zone Theory

$$
\frac{d \chi}{d t} \quad=\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
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& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\widetilde{\mathrm{C}}: \underbrace{\text { Stiffness }}_{\text {Elastic Part }} \\
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& \underbrace{\frac{d \mathbf{u}}{d t}}_{m \times a}=\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
$$

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Advective derivative

## Continuum Theory

## Linear Elasticity

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Shear Transformation Zone Theory

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\underbrace{\frac{d \chi}{d t}}_{\text {ive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
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## Linear Elasticity

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\begin{gathered}
\begin{aligned}
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& \text { Jaumann derivative }
\end{aligned} \\
\begin{aligned}
& \text { deformation } \\
& \text { D }=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
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\end{aligned}
\end{gathered}
$$

Shear Transformation Zone Theory

$$
\begin{aligned}
\frac{d \chi}{\frac{d t}{d t}} & =\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}} \\
\bar{s}^{2} & =\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}
\end{aligned}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{gathered}
\begin{aligned}
& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\widetilde{\mathrm{C}}: \underbrace{\text { Stiffness }}_{\text {Elastic Part }} \\
& \text { Jaumann derivative }
\end{aligned} \\
\begin{aligned}
& \text { deformation } \\
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&=\underbrace{\mathrm{D}^{e l}+\mathrm{D}^{p l}}_{\text {Hypoelastoplastic assumption }} \\
& \underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a}=\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
\end{gathered}
$$

## Shear Transformation Zone Theory

$$
\begin{aligned}
& \frac{d \chi}{\frac{d t}{d t}}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}} \\
&{\underset{\text { ive derivative }}{2}}_{\bar{s}^{2}}=\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}
\end{aligned}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
\begin{aligned}
& \frac{\mathcal{D} \sigma}{\mathcal{D} t}=\underbrace{\text { Stiffness }}_{\text {Jaumann derivative }}: \underbrace{\mathrm{D}^{\mathrm{Cel}}}_{\text {Elastic Part }} \\
& \text { Rate of deformation }
\end{aligned} \\
\begin{aligned}
\mathrm{D} & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& =\underbrace{\mathrm{D}^{e l}+\mathrm{D}^{p l}}_{\text {Hypoelastoplastic assumption }} \\
\underbrace{\frac{d \mathbf{u}}{d t}}_{m \times a} & =\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
\end{aligned}
$$

## Shear Transformation Zone Theory

$$
\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
{\underset{\sim}{s}}_{\bar{s}^{2}}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
& \underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}} \stackrel{\text { Stiffness }}{=} \overbrace{\text { Elastic Part }}^{\mathrm{C}}: \underbrace{\mathrm{el}}_{\text {Del }} \\
& \text { Jaumann derivative } \\
& \begin{aligned}
\text { Rate of deformation } & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& =\underbrace{\mathbf{D}^{e l}+\mathbf{D}^{p l}}_{\text {Hypoelastoplastic assumption }} \\
\underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a} & =\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
\end{aligned}
$$

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\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
{\underset{\sim}{2}}_{\bar{s}^{2}}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

$$
\sigma_{0}=\sigma-\frac{1}{3} \operatorname{Tr}(\sigma)
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
\begin{aligned}
\frac{\mathcal{D} \sigma}{\mathcal{D} t} & =\underbrace{\mathrm{C}}_{\text {Stiffness }}: \underbrace{\mathrm{D}^{\mathrm{del}}}_{\text {Elastic Part }}
\end{aligned} \\
\text { Jaumann derivative }
\end{aligned} \underbrace{}_{\underbrace{\mathrm{D}}_{\text {Rate of deformation }}}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} .
$$

## Shear Transformation Zone Theory

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\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
\underset{\text { ess }}{\stackrel{\rightharpoonup}{\sim}^{2}}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

$$
\left.\underbrace{\sigma_{0}}=\sigma-\frac{1}{3} \operatorname{Tr}(\sigma) \right\rvert\,
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
& \underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}} \stackrel{\text { Stiffness }}{=} \overbrace{\text { Elastic Part }}^{\mathrm{C}}: \underbrace{\mathrm{el}}_{\text {Del }} \\
& \text { Jaumann derivative } \\
& \begin{aligned}
\text { Rate of deformation } & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& =\underbrace{\mathrm{D}^{e l}+\mathrm{D}^{p l}}_{\text {Hypoelastoplastic assumption }}
\end{aligned} \\
& \underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a}=\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
$$

## Shear Transformation Zone Theory

$$
\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
{\underset{\sim}{2}}_{\bar{s}^{2}}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

$$
\underbrace{\sigma_{0}}_{\text {Deviatoric stress }}=\underbrace{\sigma-\frac{1}{3} \operatorname{Tr}(\sigma) \boldsymbol{I}}_{\text {Subtract hydrostatic }}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
\begin{aligned}
\frac{\mathcal{D} \sigma}{\mathcal{D} t} & =\stackrel{\text { Stiffness }}{\mathrm{C}}: \underbrace{\mathrm{D}^{\mathrm{del}}}_{\text {Elastic Part }}
\end{aligned} \\
\text { Jaumann derivative }
\end{aligned} \underbrace{\mathrm{D}}_{\text {Rate of deformation }}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} .
$$

## Shear Transformation Zone Theory

$$
\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
\underbrace{\bar{s}^{2}}_{\sim}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

$$
\begin{aligned}
\underbrace{\sigma_{0}}_{\text {Deviatoric stress }} & =\underbrace{\sigma-\frac{1}{3} \operatorname{Tr}(\sigma) \mathrm{I}}_{\text {Subtract hydrostatic }} \\
\mathbf{D}^{p l} & =D^{p l} \frac{\sigma_{0}}{\bar{s}}
\end{aligned}
$$

## Continuum Theory

## Linear Elasticity

$$
\begin{aligned}
\begin{aligned}
\frac{\mathcal{D} \sigma}{\mathcal{D} t} & =\underbrace{\mathrm{C}}_{\text {Stiffness }}: \underbrace{\mathrm{D}^{\mathrm{del}}}_{\text {Elastic Part }}
\end{aligned} \\
\text { Jaumann derivative }
\end{aligned} \underbrace{}_{\underbrace{\mathrm{D}}_{\text {Rate of deformation }}}=\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} .
$$

## Shear Transformation Zone Theory

$$
\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
$$

$$
\underbrace{\bar{s}^{2}}_{\sim_{2}^{2}}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
$$

Frobenius norm

$$
\underbrace{\sigma_{0}}_{\text {Oviatoric strocs }}=\underbrace{\sigma-\frac{1}{3} \operatorname{Tr}(\sigma) ।}
$$

$$
\text { Deviatoric stress } \underbrace{0}_{\text {subtract hydrostatic }}
$$

$$
\underbrace{\mathrm{D}^{p l}}_{\text {ate }}=D^{p l} \frac{\sigma_{0}}{\bar{s}}
$$

## Continuum Theory

## Linear Elasticity

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\begin{aligned}
& \underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}} \stackrel{\text { Stiffness }}{=} \overbrace{\text { Elastic Part }}^{\mathrm{C}}: \underbrace{\mathrm{el}}_{\text {Del }} \\
& \text { Jaumann derivative } \\
& \begin{aligned}
\text { Rate of deformation } & =\underbrace{\frac{1}{2}\left(\nabla \mathbf{u}+(\nabla \mathbf{u})^{T}\right)}_{\text {Definition }} \\
& =\underbrace{\mathbf{D}^{e l}+\mathrm{D}^{p l}}_{\text {Hypoelastoplastic assumption }}
\end{aligned} \\
& \underbrace{\rho \frac{d \mathbf{u}}{d t}}_{m \times a}=\underbrace{\nabla \cdot \sigma}_{\text {Net force }}
\end{aligned}
$$

## Shear Transformation Zone Theory

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\underbrace{\frac{d \chi}{d t}}_{\text {tive derivative }}=\underbrace{\frac{D^{p l} \bar{s}}{s_{y} c_{0}}\left(\chi_{\infty}-\chi\right)}_{\text {Relaxation to } \chi_{\infty}}
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$$
\underbrace{\bar{s}^{2}}_{\sim}=\underbrace{\frac{1}{2} \sigma_{0, i j} \sigma_{0, i j}}
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Frobenius norm

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\underbrace{\sigma_{0}}_{\text {Oviatoric strocs }}=\underbrace{\sigma-\frac{1}{3} \operatorname{Tr}(\sigma) ।}
$$

$$
\text { Deviatoric stress } \underbrace{0}_{\text {subtract hydrostatic }}
$$

$$
\underbrace{\mathrm{D}^{p l}}_{\text {Plastic rate }}=\underbrace{D^{p l} \frac{\sigma_{0}}{\bar{s}}}_{\text {deviatoric }}
$$

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit
Incompressible Navier-Stokes

From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit
Incompressible Navier-Stokes

$$
\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)
$$

## From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit
Incompressible Navier-Stokes
$\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}_{\text {Hypoelastoplastic equation }}$
Hypoelastoplastic equation

From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

$$
\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}
$$

Hypoelastoplastic equation

## Incompressible Navier-Stokes

$$
\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathbf{T}
$$

From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}_{\text {Hypoelastoplastic equation }}
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## Incompressible Navier-Stokes

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\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathrm{T}}_{\text {Navier-Stokes equation }}
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From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}_{\text {Hypoelastoplastic equation }}
$$

$$
\nabla \cdot \sigma \approx 0
$$

## Incompressible Navier-Stokes

$$
\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathbf{T}}_{\text {Navier-Stokes equation }}
$$

From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

$$
\begin{gathered}
\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}_{\text {Hypoelastoplastic equation }} \\
\underbrace{\nabla \cdot \sigma \approx 0}_{\text {Quasi-static constraint }}
\end{gathered}
$$

## Incompressible Navier-Stokes

$$
\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathbf{T}}_{\text {Navier-Stokes equation }}
$$

## From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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## Incompressible Navier-Stokes

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\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathrm{T}}_{\text {Navier-Stokes equation }}
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\nabla \cdot \mathbf{u} \approx 0
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## From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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## Incompressible Navier-Stokes

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$$
\nabla \cdot \mathbf{u} \approx 0
$$

Incompressibility constraint

## From Navier-Stokes to Hypoelastoplasticity

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}
$$

Hypoelastoplastic equation
$\underbrace{\nabla \cdot \sigma \approx 0}_{\text {Quasi-static constraint }}$

## Incompressible Navier-Stokes

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\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathbf{T}}_{\text {Navier-Stokes equation }}
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$$
\nabla \cdot \mathbf{u} \approx 0
$$

Incompressibility constraint

## From Navier-Stokes to Hypoelastoplasticity

$$
\sigma_{\text {H.E.P. }} \Longleftrightarrow \mathbf{u}_{\text {N.S. }}
$$

## A Thought-Provoking Analogy

Hypoelastoplastic Long-Time Limit

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\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}
$$

Hypoelastoplastic equation


Quasi-static constraint

## Incompressible Navier-Stokes

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\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathrm{T}}_{\text {Navier-Stokes equation }}
$$

$$
\underbrace{\nabla \cdot \mathbf{u} \approx 0}
$$

Incompressibility constraint

## From Navier-Stokes to Hypoelastoplasticity

$$
\begin{aligned}
\sigma_{\text {H.E.P. }} & \Longleftrightarrow \mathrm{u}_{\text {N.S. }} \\
& \mathrm{u}_{\text {H.E.P. }}
\end{aligned} \Longleftrightarrow p_{\text {N.S. }} .
$$

## A Thought-Provoking Analogy

## Hypoelastoplastic Long-Time Limit

$$
\underbrace{\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\mathrm{C}:\left(\mathrm{D}-\mathrm{D}^{\mathrm{pl}}\right)}
$$

Hypoelastoplastic equation

$$
\nabla \cdot \sigma \approx 0
$$

Quasi-static constraint

## Incompressible Navier-Stokes

$$
\underbrace{\rho \frac{d \mathbf{u}}{d t}=-\nabla p+\nabla \cdot \mathbf{T}}_{\text {Navier-Stokes equation }}
$$

$$
\underbrace{\nabla \cdot \mathrm{u} \approx 0}
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Incompressibility constraint

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\end{gathered}
$$

From Navier-Stokes to Hypoelastoplasticity


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\begin{aligned}
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- Any algorithm for Navier-Stokes should work for hypoelastoplasticity.


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- This analogy is independent of the plasticity model.


## A Quasi-Static Projection Method

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\frac{\sigma^{*}-\sigma^{n}}{\Delta t}=-\sigma^{n} \cdot \omega^{n}+\omega^{n} \cdot \sigma^{n}-\left(\mathbf{u}^{n} \cdot \nabla\right) \sigma^{n}-\mathbf{C}:\left[\mathrm{D}^{\mathrm{pl}}\right]^{n}
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Forward-Euler intermediate step

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\underbrace{\frac{\sigma^{*}-\sigma^{n}}{\Delta t}}_{\text {intermediate step }}=\underbrace{-\sigma^{n} \cdot \omega^{n}+\omega^{n} \cdot \sigma^{n}}_{\text {Jaumann spin terms }}-\left(\mathbf{u}^{n} \cdot \nabla\right) \sigma^{n}-\mathrm{C}: \overbrace{[\mathrm{D} \mathrm{pl}]^{n}}
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Forward-Euler intermediate step

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- Take divergence and enforce $\nabla \cdot \sigma^{n+1}=0$ :


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- Solve the above equation using the multigrid method for the velocities $\mathbf{u}^{n+1}$.


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- Solve the above equation using the multigrid method for the velocities $\mathbf{u}^{n+1}$.
- Apply the projection step to compute $\sigma^{n+1}$.


## stzpp

- Same software for both quasi-static and explicit method.


## stzpp

- Same software for both quasi-static and explicit method.
- Staggered grid: $\sigma, \chi$ at cell centers. u at cell corners.


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- Parallelized using domain decomposition and MPI.



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- Ghost-regions pad processor subdomains with two points.



## Projection Step

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- Need to solve complex linear system with mixed spatial derivatives for velocity update.


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$$
\mathbf{x}=\left(\begin{array}{c}
\vdots \\
\left(\begin{array}{c}
u_{i-1, j, k}^{n+1} \\
v_{i-1, j, k}^{n+1} \\
w_{i-1, j, k}^{n+1}
\end{array}\right) \\
\left(\begin{array}{c}
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- Gauss-Seidel:

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x_{i}^{k+1}=\frac{1}{a_{i i}}\left(b_{i}-\sum_{j=1}^{i-1} a_{i j} x_{j}^{k+1}-\sum_{j=i+1}^{n} a_{i j} x_{j}^{k}\right)
$$

$$
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superscript: iteration count
$\overbrace{x_{i}^{k+1}}^{\frac{1}{a_{i i}}}\left(b_{i}-\sum_{j=1}^{i-1} a_{i j} x_{j}^{k+1}-\sum_{j=i+1}^{n} a_{i j} x_{j}^{k}\right)$
subscript: element index

$$
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| :---: |
| $\mathrm{~T}_{3}$ |
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Grid
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## Quasi-Static Results

## Conclusions, Future Directions, and Acknowledgments

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- Numerical extensions to the QS algorithm can be made by considering work in computational fluid dynamics (e.g. gauge methods).


## Conclusions, Future Directions, and Acknowledgments

- Metallic glasses: a promising new class of materials with diverse technological and structural applications and interesting physics.
- Shear banding, a poorly understood failure mechanism, limits their applications.
- Quasi-static projection algorithm enables simulation of large systems at long timescales by exploiting an analogy to the incompresible Navier-Stokes equations.
- Numerical extensions to the QS algorithm can be made by considering work in computational fluid dynamics (e.g. gauge methods).
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[^0]:    $\frac{\mathcal{D} \sigma}{\mathcal{D} t}=\stackrel{\text { Stiffness }}{\widetilde{\mathrm{C}}}: \underbrace{\mathrm{Del}}_{\text {Elastic Part }}$
    Jaumann derivative

